



Title	<i>Reference Design Report for a 7 W, Wide Range Input, Dual Output, Non-Isolated Flyback Converter Using LinkSwitch™-XT2-900 LNK3696P</i>
Specification	85 VAC – 440 VAC Input; 12.0 V / 500 mA, 5.0 V / 200 mA Outputs
Application	Embedded Power Supply
Author	Applications Engineering Department
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Revision	1.2

Summary and Features

- Highly integrated solution with 900 V rated power MOSFET
- Output voltage regulation: 12 V \pm 10%, 5 V \pm 5%
- Programmable current limit selection feature of LinkSwitch-XT2-900
- Extremely fast transient response independent of load timing
- >80% efficiency at full load condition
- <120 mW no-load input power at 230 VAC
- >6 dB conducted EMI margin
- No optocoupler or Zener diode required for regulation
- Can withstand up to 450 VAC line input

PATENT INFORMATION

The products and applications illustrated herein (including transformer construction and circuits external to the products) may be covered by one or more U.S. and foreign patents, or potentially by pending U.S. and foreign patent applications assigned to Power Integrations. A complete list of Power Integrations' patents may be found at www.powerint.com. Power Integrations grants its customers a license under certain patent rights as set forth at <https://www.power.com/company/intellectual-property-licensing/>.

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Important Note:

Although this board is designed to satisfy safety isolation requirements, the engineering prototype has not been agency approved. Therefore, all testing should be performed using an isolation transformer to provide the AC input to the prototype board.



1 Introduction

This engineering report describes a non-isolated flyback converter designed to provide dual output of 5 V at 200 mA and 12 V at 500 mA from a wide input voltage range of 85 VAC to 440 VAC. This adapter utilizes the LNK3696P from the LinkSwitch-XT2 900 V family of devices.

This document contains the power supply specification, schematic, bill of materials, transformer documentation, printed circuit layout, and performance data.

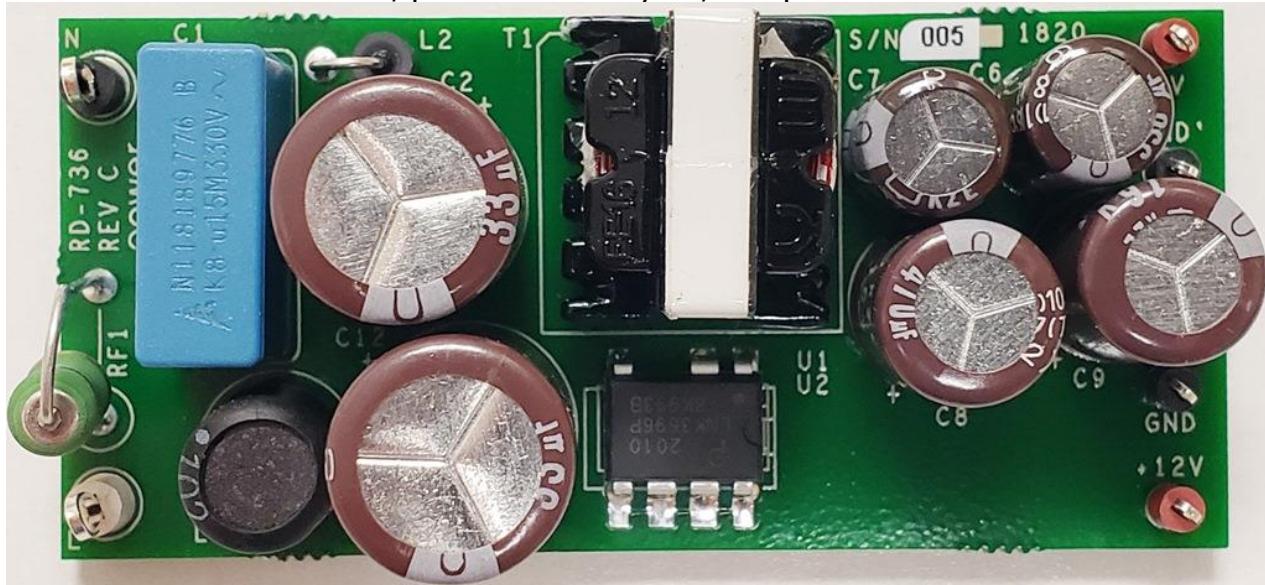


Figure 1 – Populated Circuit Board Photograph, Top.

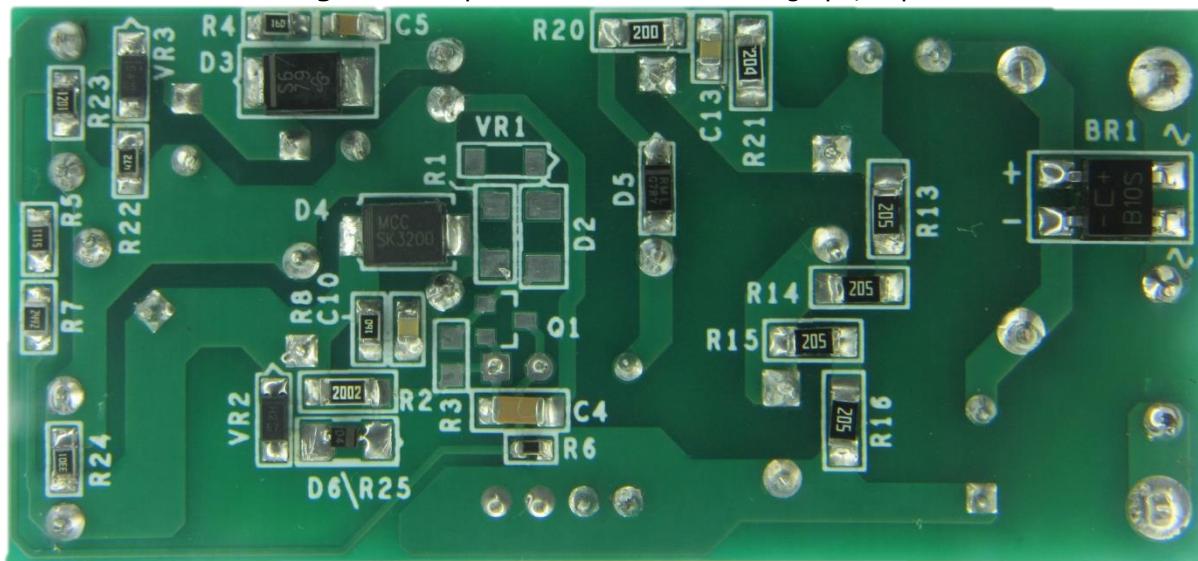


Figure 2 – Populated Circuit Board Photograph, Bottom.



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2 Power Supply Specification

The table below represents the minimum acceptable performance of the design. Actual performance is listed in the results section.

Description	Symbol	Min	Typ	Max	Units	Comment
Input						
Voltage	V_{IN}	85		440	VAC	2 Wire – no P.E. Verified at 450 VAC.
Frequency	f_{LINE}	50	50/60	60	Hz	
No-load Input Power				200	mW	230 VAC.
Output						
Output Voltage 1	V_{OUT-5}	4.75	5.0	5.25	V	±5%
Output Current 1	I_{OUT-5}	50	200		mA	
Output Voltage 2	V_{OUT-12}	10.8	12.0	13.2	V	±10%
Output Current 2	I_{OUT-12}	50	500		mA	
Output Ripple Voltage	V_{RIPPLE}			200	mV	20 MHz Bandwidth.
Output Power	P_{OUT}		7		W	
Efficiency						
Full Load	η_{Full-Load}		80		%	Measured at Output Terminal.
Environmental						
Conducted EMI			CISPR22B / EN55022B			Resistive Load, 6 dB Margin.
Line Surge			Load floating			
Differential Mode (L/N)				1	kV	Differential: 2 Ω
Ambient Temperature	T_{AMB}	0		40	°C	Free Convection, Sea Level in Sealed Enclosure.

3 Schematic

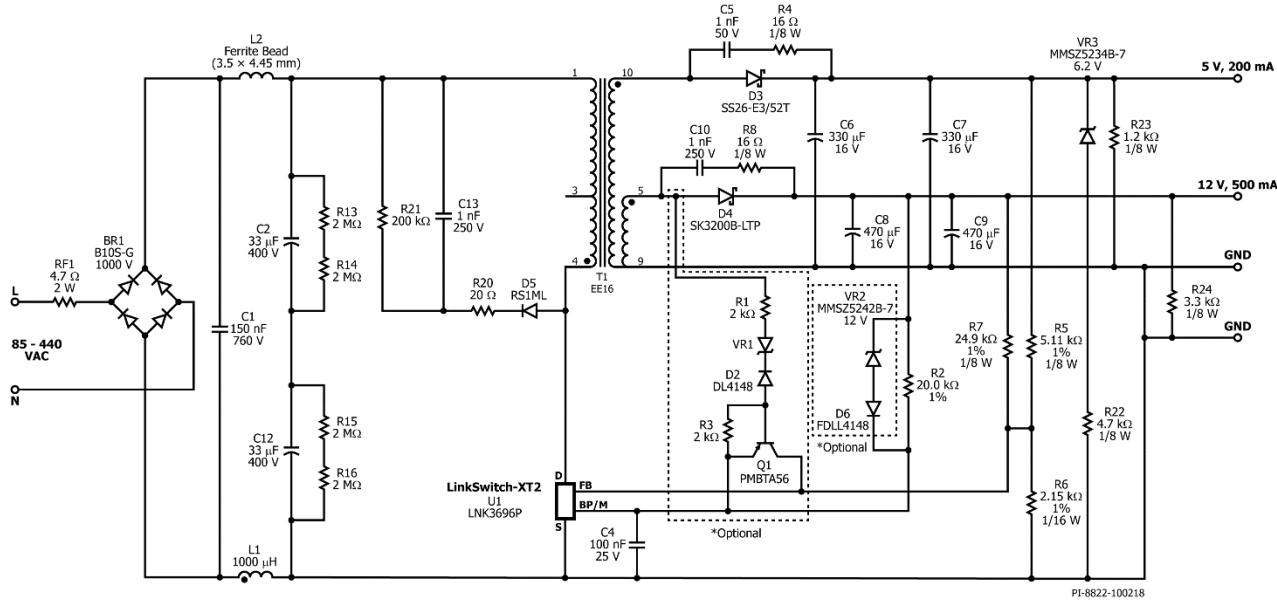


Figure 3 – Schematic.



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4 Circuit Description

The LinkSwitch-XT2 900 V family of devices integrates a high-voltage (900 V rated) power MOSFET with an internal oscillator and ON/OFF controller inside a single monolithic IC. Unlike conventional pulse width modulation (PWM) controllers, LinkSwitch-XT2 900 V devices utilize a simple ON/OFF control scheme combined with an internal current limit circuitry to regulate the output voltage. The LNK3696P IC was used in a non-isolated flyback with dual output (12 V and 5 V) delivering 500 mA and 200 mA respectively.

4.1 Input Rectifier and Filter

The AC input is rectified by bridge rectifier BR1 and filtered by the bulk storage capacitors C2 and C3. Resistor RF1 is a flameproof, fusible, wire wound type and functions as a fuse, inrush current limiter and, together with the filter formed by C1, C2, C3, L1 and L2, differential mode noise attenuator. Resistors R13, R14, R15 and R16 function to balance the voltage between the bulk capacitors in series.

4.2 LinkSwitch-XT2 Primary-Side

The rectified and filtered input voltage is applied to the primary winding of flyback transformer T1. T1 is switched and connected to the IC via the DRAIN (D) pin. The D pin provides internal operating current for both start-up and steady-state operating conditions.

During the power MOSFET turn on time, current ramps up in the primary winding, storing energy inside the transformer core, while the two secondaries remain cut-off due to reverse biasing of the diodes. The primary winding current eventually exceeds the internal threshold (I_{LIMIT}), causing the power MOSFET to turn off for the remainder of the switching cycle. At the beginning of the next and all succeeding switching cycles, the IC decides whether to turn ON the power MOSFET or let it remain turned OFF. ON/OFF control is performed by comparing the output voltage to the reference voltage V_{FB} , resulting to the power MOSFET being enabled or disabled. Through the use of ON/OFF control, voltage regulation is maintained by skipping cycles without using an error amplifier and ramp generator, as in traditional power supply controllers.

4.3 Primary RCD Clamp

A low cost RCD clamp is connected across the primary winding of transformer T1. This is composed of resistors R20 and R13, capacitor C13 and diode D5. The clamp helps in dissipating the energy stored in the leakage inductance of T1.

4.4 Output Rectification

Transformer T1 has two secondary windings on its core – one for each output voltage. For both secondaries, the secondary switching voltage is rectified by Schottky diodes D3 and D4, and then filtered by super low ESR type capacitors C6, C7, C8 and C9. For each

Schottky diode, a snubber network is connected in parallel using resistors R4 and R8, and capacitors C5 and C10. The snubber network helps limit the peak inverse voltage spikes seen by the diode. Pre-load resistors R23 and R23 are connected on each output to improve cross-regulation performance.

4.5 Output Feedback

The two outputs 12 V and 5 V are sensed through resistor dividers R5, R6 and R7. The sensed voltage is fed back to U1 through the FEEDBACK (FB) pin. This voltage V_{FB} must be accurately maintained at 2 V, so the sensing resistors must have 1% tolerance.

A weighted feedback circuit using resistors R5, R6 and R7 are connected to both output voltages and into the FB pin. The magnitude of the weights are determined by the relative contributions of current delivered into the FB pin, which then determine the values of R5 and R7. In the schematic, a larger current is contributed by the 5 V output, due to the larger current through R5 as compared to R7. Effectively, the 5 V output voltage has better feedback sensitivity and output regulation.

4.6 Output Overvoltage Protection

The BYPASS (BP/M) pin has multiple functions: it provides a connection point for an external bypass capacitor as well current limit value selector via the capacitance value, and it provides a shutdown function. Similar to the FB pin, when the current delivered into the BP/M pin exceeds the internal threshold ($I_{BP(SD)}$) for a time equal to 2 to 3 cycles of the switching frequency, the device enters auto-restart. By designing a circuit that injects current into the BP/M pin due to a fault, the device can be equipped with both output overvoltage and line overvoltage protection.

For the 5 V output, a simple clamp circuit using Zener diode VR3 and resistor R22 is used for overvoltage protection. For the 12 V output, Zener diode VR2, diode D6 and resistor R7 comprise the overvoltage protection circuit. A voltage at the 12 V output exceeds the sum of the VR2 voltage rating, D2 diode drop, and the bypass voltage will cause a current in excess of $I_{BP(SD)}$ to be injected into the BP/M pin, which will trigger the auto-restart and protect the power supply from overvoltage.

4.7 Line Overvoltage Protection

The device indirectly senses the DC bus voltage by sampling the secondary voltage during the power MOSFET on-time. During this time, the voltage across the secondary winding is proportional to the voltage across the primary winding. When the DC bus voltage exceeds the limit, Zener diode VR1 and diode D2 are turned on causing current to flow through transistor Q1 and into the FB pin. The device will go into auto-restart mode if the FB pin current limit is exceeded for at least 2 consecutive switching cycles.



5 PCB Layout

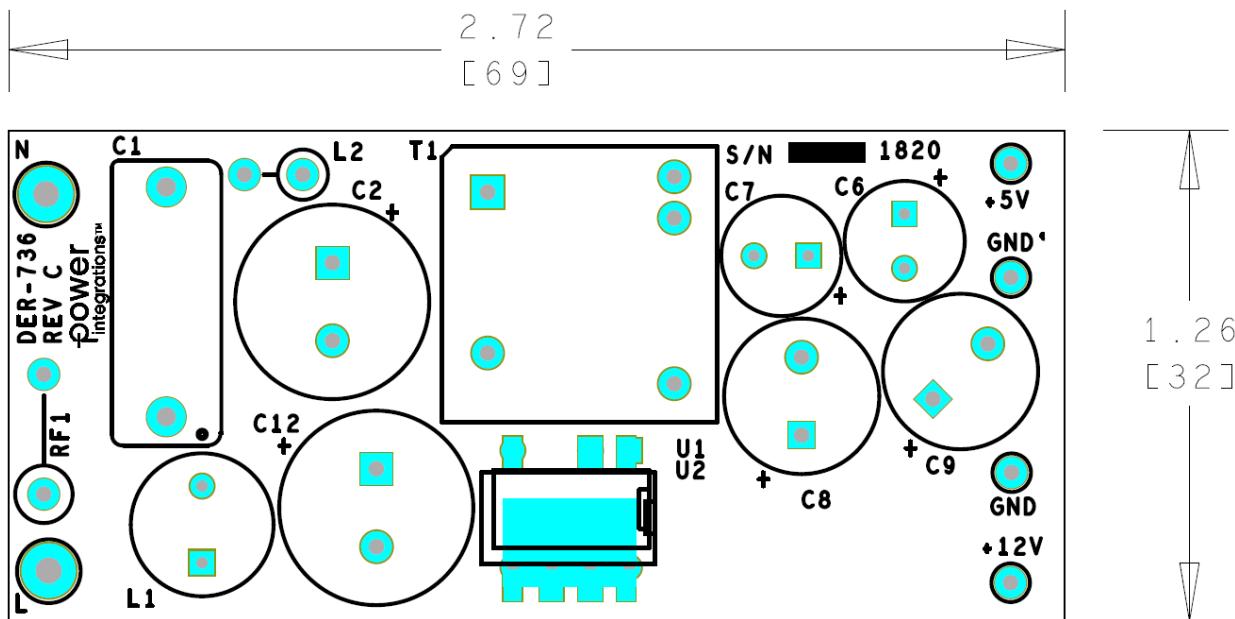


Figure 4 – Printed Circuit Layout, Top.

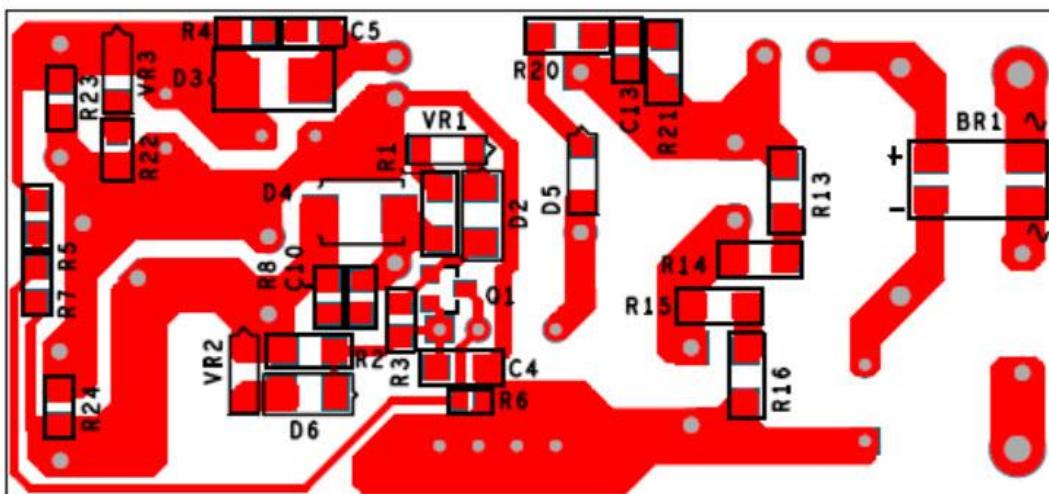


Figure 5 – Printed Circuit Layout, Bottom.

6 Bill of Materials

Item	Qty	Ref Des	Description	Mfg Part Number	Mfg
1	1	BR1	1000 V, 0.8 A, Bridge Rectifier, SMD, MBS-1, 4-SOIC	B10S-G	Comchip
2	1	C1	150 nF, 760 V, Polypropylene Film	B32912B3154M	Epcos
3	2	C2 C12	33 µF, 400 V, Electrolytic, (12.5 x 20)	KMG401ELL330MK20S	Nippon Chemi-Con
4	1	C4	100 nF, 25 V, Ceramic, X7R, 1206	C1206F104K3RACTU	Kemet
5	1	C5	1 nF, 50 V, Ceramic, X7R, 0805	08055C102KAT2A	AVX
6	2	C6 C7	330 µF, 16 V, Electrolytic, Very Low ESR, 72 mΩ, (8 x 11.5)	EKZE160ELL331MHB5D	Nippon Chemi-Con
7	2	C8 C9	470 µF, 16 V, Electrolytic, Very Low ESR, 53 mΩ, (10 x 12.5)	EKZE160ELL471MJC5S	Nippon Chemi-Con
8	2	C10 C13	1 nF, 250 V, Ceramic, X7R, 0805	GRM21AR72E102KW01D	Murata
9	1	D3	60 V, 2 A, Schottky, SMD, DO-214AA	SS26-E3/52T	Vishay
10	1	D4	200 V, 3 A, DIODE SCHOTTKY 1A 200 V, SMB	SK3200B-LTP	Micro Commercial
11	1	D5	1000 V, 800 mA, Fast Recovery SMF, 5000 ns,	RS1ML	Taiwan Semi
12	1	D6	100 V, 10 mA, Fast Switching, 4 ns, MINI-MELF, SOD-80	FDLL4148	ON Semi
13	1	L1	1000 µH, 0.510 A	RLB9012-102KL	Bourns
14	1	L2	3.5 mm x 4.45 mm, 56 Ω at 100 MHz, #22 AWG hole, Ferrite Bead	2761001112	Fair-Rite
15	1	R2	RES, 20.0 kΩ, 1%, 1/4 W, Thick Film, 1206	ERJ-8ENF2002V	Panasonic
16	2	R4 R8	RES, 16 Ω, 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ160V	Panasonic
17	1	R5	RES, 5.11 kΩ, 1%, 1/8 W, Thick Film, 0805	ERJ-6ENF5111V	Panasonic
18	1	R6	RES, 2.15 kΩ, 1%, 1/16 W, Thick Film, 0603	ERJ-3EKF2151V	Panasonic
19	1	R7	RES, 24.9 kΩ, 1%, 1/8 W, Thick Film, 0805	ERJ-6ENF2492V	Panasonic
20	4	R13 R14 R15 R16	RES, 2 MΩ, 5%, 1/4 W, Thick Film, 1206	ERJ-8GEYJ205 V	Panasonic
21	1	R20	RES, 20 Ω, 5%, 1/4 W, Thick Film, 1206	ERJ-8GEYJ200V	Panasonic
22	1	R21	RES, 200 kΩ, 5%, 1/4 W, Thick Film, 1206	ERJ-8GEYJ204V	Panasonic
23	1	R22	RES, 4.7 kΩ, 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ472V	Panasonic
24	1	R23	RES, 1.2 kΩ, 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ122V	Panasonic
25	1	R24	RES, 3.3 kΩ, 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ332V	Panasonic
26	1	RF1	RES, 4.7 Ω, 2 W, Flame Proof, Pulse Withstanding, Wire Wound	FW20A4R70JA	Bourns.
27	1	T1	Bobbin, EE16, Vertical, 10 pins (4 x 6)	EL-16 (YW-193-02B)	Yih-Hwa
28	1	U1	LinkSwitch-XT2-900, DIP-8C	LNK3696P	Power Integrations
39	1	VR2	DIODE ZENER 12 V 500 mW SOD123	MMSZ5242B-7-F	Diodes, Inc.
30	1	VR3	DIODE ZENER 6.2 V 500 mW SOD123	MMSZ5234B-7-F	Diodes, Inc.

Miscellaneous Parts

Item	Qty	Ref Des	Description	Mfg Part Number	Mfg
1	2	GND GND`	Test Point, BLK,Miniature THRU-HOLE MOUNT	5001	Keystone
2	2	+5V, +12V	Test Point, RED,Miniature THRU-HOLE MOUNT	5000	Keystone
3	1	L	Test Point, WHT,THRU-HOLE MOUNT	5012	Keystone
4	1	N	Test Point, BLK,THRU-HOLE MOUNT	5011	Keystone



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7 Transformer Specification

7.1 Electrical Diagram

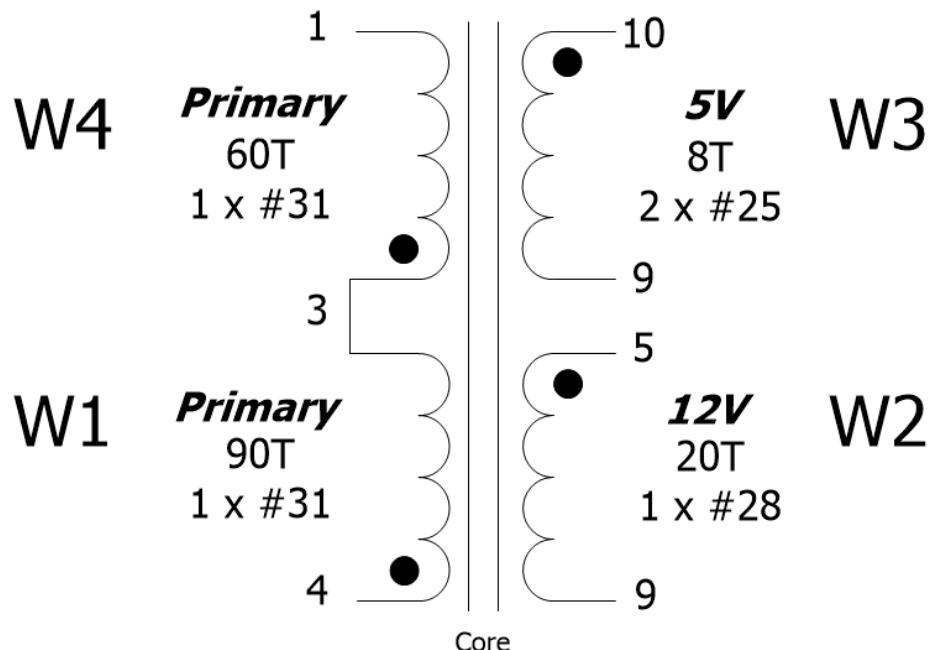


Figure 6 – Transformer Electrical Diagram.

7.2 Electrical Specifications

Parameter	Condition	Spec
Electrical Strength	60 Hz, 1 second, from pins 1-4 to pins 9-10	3000 VAC
Primary Inductance	Pins 1-4, all other windings open, measured at 100 kHz, 0.4 V _{RMS} .	1500 μ H $\pm 7\%$
Primary Leakage Inductance	Pins 1-4, all other windings short, measured at 100 kHz, 0.4 V _{RMS} .	<100 μ H

7.3 Material List

Item	Description
[1]	Core: EE16, Gapped.
[2]	Bobbin: EE16, Vertical, 10 pins.
[3]	Magnet Wire: #31 AWG.
[4]	Magnet Wire: #28 AWG.
[5]	Magnet Wire: #25 AWG.
[6]	Tape, 3M 1298 Polyester Film, 2.0 Mils Thick, 8.4 mm Wide.
[7]	Tape, 3M 1298 Polyester Film, 2.0 Mils Thick, 4.5 mm Wide.
[8]	Varnish.

7.4 Transformer Build Diagram

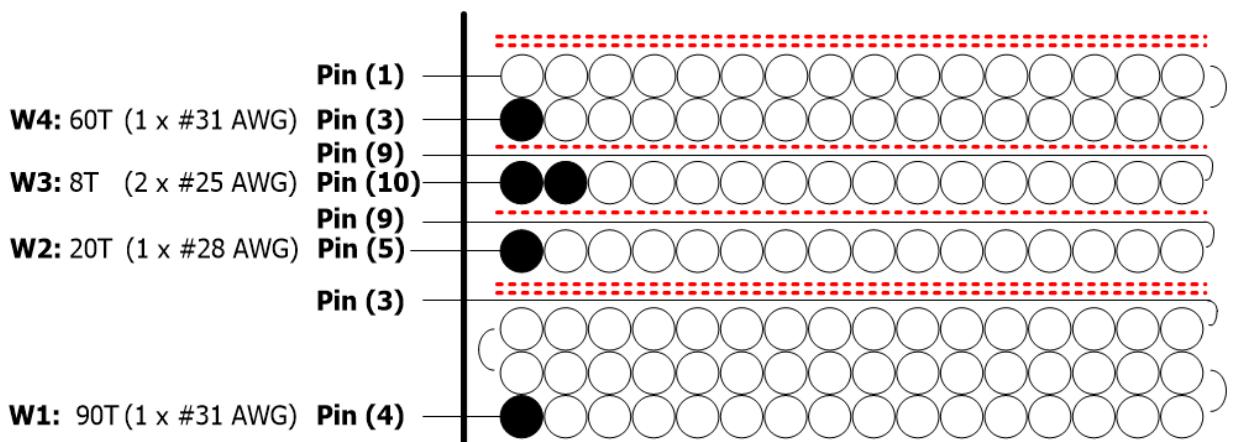
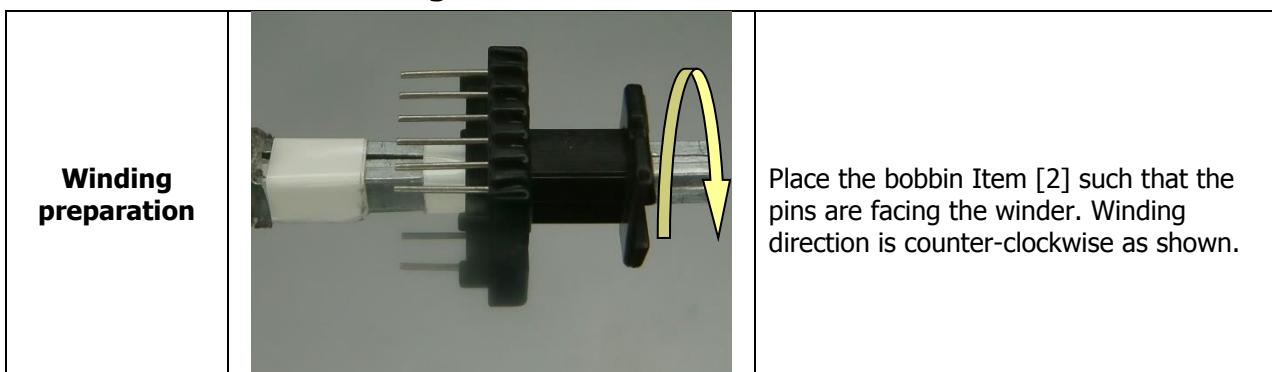


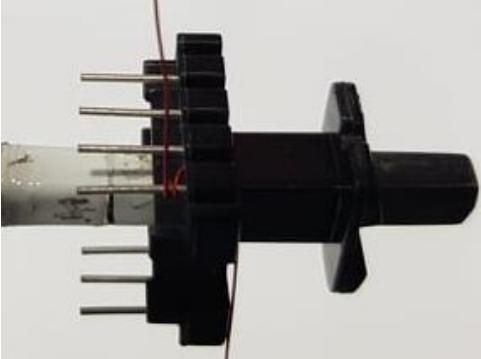
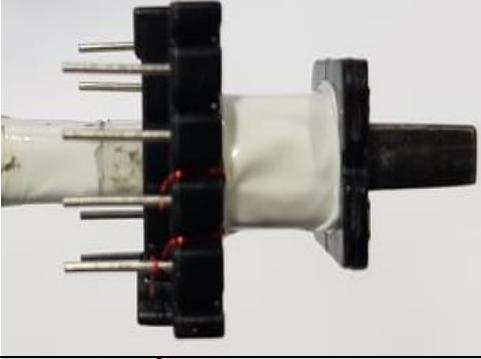
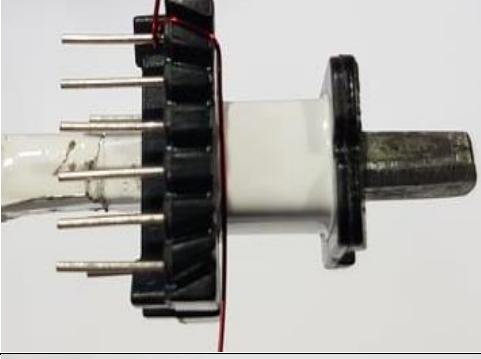
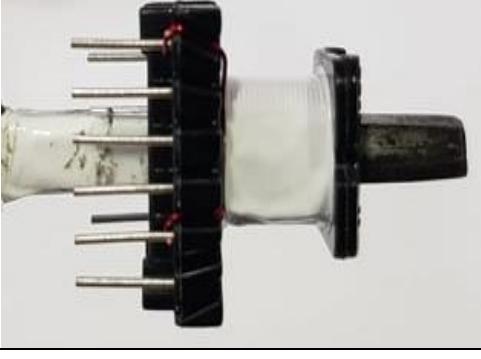
Figure 7 – Transformer Build Diagram.

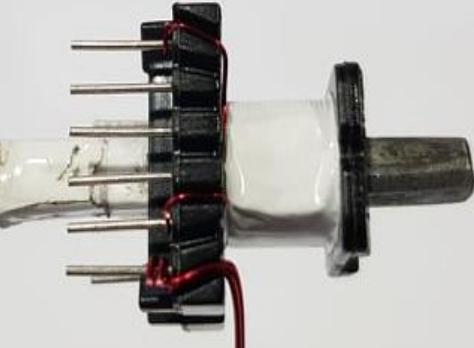
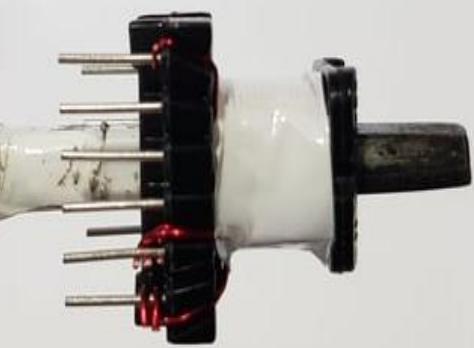
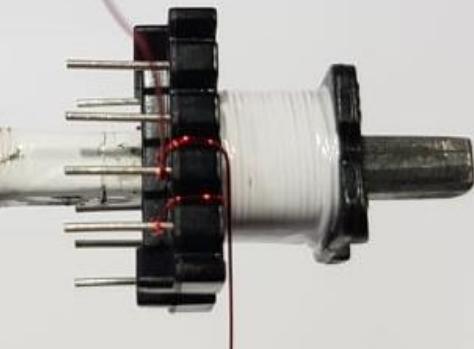
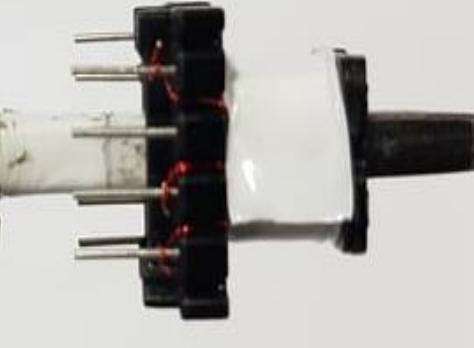
7.5 Transformer Construction

Winding preparation	Place the bobbin Item [2] such that the pins are facing the winder. Winding direction is counter-clockwise as shown.
W1 1st Primary	Starting at pin 4, wind 90 turns of wire Item [3] in three layers. At the last turn, bring the wire back across the windings and into pin 3.
Insulation	Apply two layers of tape Item [6] for insulation.
W2 12V Winding	Start at pin 5, wind 20 turns of wire Item [4] in one layer. At the last turn, bring the wire back across the windings and into pin 9.
Insulation	Use 1 layer of tape Item [6] for insulation.
W3 5V Winding	Starting at pin 10, wind 7.7 turns of two strands of wire Item [5] in one layer. At the last turn, bring the wire back across the windings and into pin 9.
Insulation	Use 1 layer of tape Item [6] for insulation.
W4 2nd Primary	Continue the primary winding at pin 3. Wind 60 turns of wire Item [3] in two layers. Finish at pin 1.
Insulation	Apply two layers of tape Item [6] for insulation.
Assembly	Grind core halves for specified primary inductance, insert bobbin, and secure core halves with tape Item [7]. Cut pin 3 short. Remove pins 2, 6, 7 and 8. Dip varnish.

7.6 Transformer Winding Illustrations



W1 1st Primary		Starting at pin 4, wind 90 turns of wire Item [3] in three layers. At the last turn, bring the wire back across the windings and into pin 3.
Insulation		Apply two layers of tape Item [6] for insulation.
W2 12V Winding		Start at pin 5, wind 20 turns of wire Item [4] in one layer. At the last turn, bring the wire back across the windings and into pin 9.
Insulation		Use 1 layer of tape Item [6] for insulation.

W3 5V Winding		Starting at pin 10, wind 8 turns of two strands of wire Item [5] in one layer. At the last turn, bring the wire back across the windings and into pin 9.
Insulation		Use 1 layer of tape Item [6] for insulation.
W4 2nd Primary		Continue the primary winding at pin 3. Wind 60 turns of wire Item [3] in two layers. Finish at pin 1.
Insulation		Apply two layers of tape Item [6] for insulation.



Assembly		<p>Grind core halves for specified primary inductance, insert bobbin, and secure core halves with tape Item [7].</p> <p>Cut pin 3 short.</p> <p>Remove pins 2, 6, 7 and 8.</p> <p>Dip varnish.</p>
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8 Transformer Design Spreadsheet

Note: The output current entered in the spreadsheet was increased such that POUT matches the combined power of the dual outputs.

<i>ACDC_LinkSwitchXT290 0V_092018; Rev.1.1; Copyright Power Integrations 2018</i>		<i>INPUT</i>	<i>INFO</i>	<i>OUTPUT</i>	<i>UNIT</i>	<i>ACDC_LinkSwitchXT2 900V Flyback Design Spreadsheet</i>
ENTER APPLICATION VARIABLES						
LINE VOLTAGE RANGE			UNIVERSAL			AC line voltage range
VACMIN	85.00		85.00	Volts		Minimum AC line voltage
VACTYP	115.00		115.00	Volts		Typical AC line voltage
VACMAX	440.00		440.00	Volts		Maximum AC line voltage
fL			50	Hertz		AC mains frequency
TIME_BRIDGE_CONDUCTIO N			2.87	mseconds		Input bridge rectifier diode conduction time
LINE RECTIFICATION			F			Select 'F'ull wave rectification or 'H'alf wave rectification
VOUT	12.00		12.00	Volts		Output voltage
IOUT	0.600		0.600	Amperes		Average output current specification
EFFICIENCY	0.80		0.80			Efficiency Estimate at output terminals. Under 0.8 if no better data available
LOSS ALLOCATION FACTOR			0.50			The ratio of power losses during the MOSFET off-state to the total system losses
POUT			7.20	Watts		Continuous Output Power
CIN	16.50		16.50	uFarads		Input capacitor
VMIN			79.59	Volts		Valley of the rectified VACMIN
VMAX			622.25	Volts		Peak of the VACMAX
FEEDBACK	MAIN		MAIN			Select the type of feedback required. (MAIN = feedback via Main Output - Non-isolated)
BIAS WINDING			NO			Select whether a bias winding is required
LINKSWITCH-XT2 VARIABLES						
CURRENT LIMIT MODE			STD			Pick between 'RED' (Reduced) or 'STD' (Standard) current limit mode of operation
PACKAGE			DIP-8C			Device package
ENCLOSURE			OPEN FRAME			Device enclosure
GENERIC DEVICE	LNK3696		LNK3696			Device series
DEVICE CODE			LNK3696P			Device code
PMAX			8.00	Watts		Device maximum power capability
VOR	95		95	Volts		Voltage reflected to the primary winding when the MOSFET is off
VDSON			10.0	Volts		MOSFET on-time drain to source peak voltage
VDSOFF			841.8	Volts		The off-time drain to source voltage is higher than 90% of the device breakdown voltage (900V)
ILIMITMIN			0.446	Amperes		Minimum current limit
ILIMITTYP			0.482	Amperes		Typical current limit
ILIMITMAX			0.518	Amperes		Maximum current limit
FSMIN			62000	Hertz		Minimum switching frequency
FSTYP			66000	Hertz		Typical switching frequency
FSMAX			70000	Hertz		Maximum switching frequency
RDSON			9.70	Ohms		MOSFET drain to source resistance at 25degC
PRIMARY WAVEFORM PARAMETERS						
MODE OF OPERATION			CCM			Mode of operation
KRP/KDP			0.995			Measure of continuous/discontinuous



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					mode of operation
KP_TRANSIENT		0.698			KP under conditions of a transient
DMAX		0.577			Maximum duty cycle at VMIN
TIME_ON	9.310	useconds			MOSFET conduction time at the minimum line voltage
TIME_ON_MIN	1.076	useconds			MOSFET conduction time at the maximum line voltage
IAVG_PRIMARY	0.129	Amperes			Average input current
IRMS_PRIMARY	0.196	Amperes			Root mean squared value of the primary current
LPRIMARY_MIN	1314	uH			Minimum primary inductance
LPRIMARY_TYP	1460	uH			Typical primary inductance
LPRIMARY_MAX	1606	uH			Maximum primary inductance
LPRIMARY_TOL	10				Tolerance of the Primary inductance
SECONDARY WAVEFORM PARAMETERS					
IPEAK_SECONDARY	3.885	Amperes			Peak secondary current
IRMS_SECONDARY	1.462	Amperes			Root mean squared value of the secondary current
PIV_SECONDARY	94.97	Volts			Peak inverse voltage on the secondary diode, not including the leakage spike
VF_SECONDARY	0.70	Volts			Secondary diode forward voltage drop
TRANSFORMER CONSTRUCTION PARAMETERS					
Core selection					
CORE	EE16	EE16			Select the transformer core
BOBBIN		B-EE16-H			Bobbin name
AE	19.20	mm^2			Cross sectional area of the core
LE	35.00	mm			Effective magnetic path length of the core
AL	1140.0	nH/(turns^2)			Ungapped effective inductance of the core
VE	795.0	mm^3			Volume of the core
AW	14.76	mm^2			Window area of the bobbin
BW	8.50	mm			Width of the bobbin
MLT	0.00	mm			Mean length per turn of the bobbin
MARGIN	0.00	mm			Safety margin
Primary winding					
NPRIMARY	150				PrImary number of turns
BMAX_TARGET	1500	Gauss			Target value of the magnetic flux density
BMAX_ACTUAL	2625	Gauss			The actual flux density of the device has been exceeded
BAC	1306	Gauss			AC flux density
ALG	65	nH/T^2			Gapped core effective inductance
LG	0.351	mm			Core gap length
LAYERS_PRIMARY	4				Number of primary layers
AWG_PRIMARY	33				Primary winding wire AWG
OD_PRIMARY_INSULATED	0.219	mm			Primary winding wire outer diameter with insulation
OD_PRIMARY_BARE	0.180	mm			Primary winding wire outer diameter without insulation
CMA_PRIMARY	256	mil^2/Amper es			Primary winding wire CMA
Secondary winding					
NSECONDARY	20	20			Secondary turns
AWG_SECONDARY		25			Secondary winding wire AWG
OD_SECONDARY_INSULATED	0.760	mm			Secondary winding wire outer diameter with insulation
OD_SECONDARY_BARE	0.455	mm			Secondary winding wire outer diameter without insulation
CMA_SECONDARY	219	mil^2/Amper es			Secondary winding CMA
Bias winding					



NBIAS			N/A		Bias turns
VF_BIAS			N/A	Volts	Bias diode forward voltage drop
VBIAS			N/A	Volts	Bias winding voltage
PIVB			N/A	Volts	Peak inverse voltage on the bias diode
CBP			0.1	uF	BP pin capacitor
FEEDBACK PARAMETERS					
DIODE_BIAS			1N4003-4007		Recommended diode is 1N4003. Place diode on return leg of bias winding for optimal EMI
RUPPER			15000	ohms	CV bias resistor for CV/CC circuit. See LinkSwitch-XT2 Design Guide
RLOWER			3000	ohms	Resistor to set CC linearity for CV/CC circuit. See LinkSwitch-XT2 900V Design Guide
MULTIPLE OUTPUT PARAMETERS					
Output 1					
VOUT1			12.00	Volts	Output Voltage 1
IOUT1			0.600	Amperes	Output Current 1
POUT1			7.20	Watts	Output Power 1
VD1			0.70	Volts	Secondary diode forward voltage drop for output 1
NS1			20		Number of turns for output 1
ISRMS1			1.462	Amperes	Root mean squared value of the secondary current for output 1
IRIPPLE1			1.333	Amperes	Current ripple on the secondary waveform for output 1
PIV1			94.97	Volts	Peak inverse voltage on the secondary diode for output 1
DIODE1_RECOMMENDED			BYV27-200		Recommended diode for output 1
PRELOAD			6.04	kohms	Preload resistor to ensure a load of at least 3mA on the first output for BIAS, 2mA for MAIN
CMS1			292.4	Cmils	Bare conductor effective area in circular mils for output 1
AWGS1			25	AWG	Wire size for output 1
Output 2					
VOUT2	5.00		5.00	Volts	Output Voltage 2
IOUT2	0.200		0.200	Amperes	Output Current 2
POUT2			1.00	Watts	Output Power 2
VD2			0.70	Volts	Secondary diode forward voltage drop for output 2
NS2			9		Number of turns for output 2
ISRMS2			0.487	Amperes	Root mean squared value of the secondary current for output 2
IRIPPLE2			0.444	Amperes	Current ripple on the secondary waveform for output 2
PIV2			42.34	Volts	Peak inverse voltage on the secondary diode for output 2
DIODE2_RECOMMENDED			SB160		Recommended diode for output 2
CMS2			97.5	Cmils	Bare conductor effective area in circular mils for output 2
AWGS2			30	AWG	Wire size for output 2
Output 3					
VOUT3			0.00	Volts	Output Voltage 3
IOUT3			0.000	Amperes	Output Current 3
POUT3			0.00	Watts	Output Power 3
VD3			0.70	Volts	Secondary diode forward voltage drop for output 3
NS3			2		Number of turns for output 3
ISRMS3			0.000	Amperes	Root mean squared value of the secondary current for output 3
IRIPPLE3			0.000	Amperes	Current ripple on the secondary



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					waveform for output 3
PIV3			8.30	Volts	Peak inverse voltage on the secondary diode for output 3
DIODE3_RECOMMENDED			NA		Recommended diode for output 3
CMS3			0.0	Cmils	Bare conductor effective area in circular mils for output 3
AWGS3			0	AWG	Wire size output for 3
PO_TOTAL			8.20	Watts	The total power of all outputs exceeds the design power
NEGATIVE OUTPUT			N/A		If negative output exists, enter the output number; e.g. If VO2 is negative output, select 2



9 Performance Data

9.1 No-Load Input Power

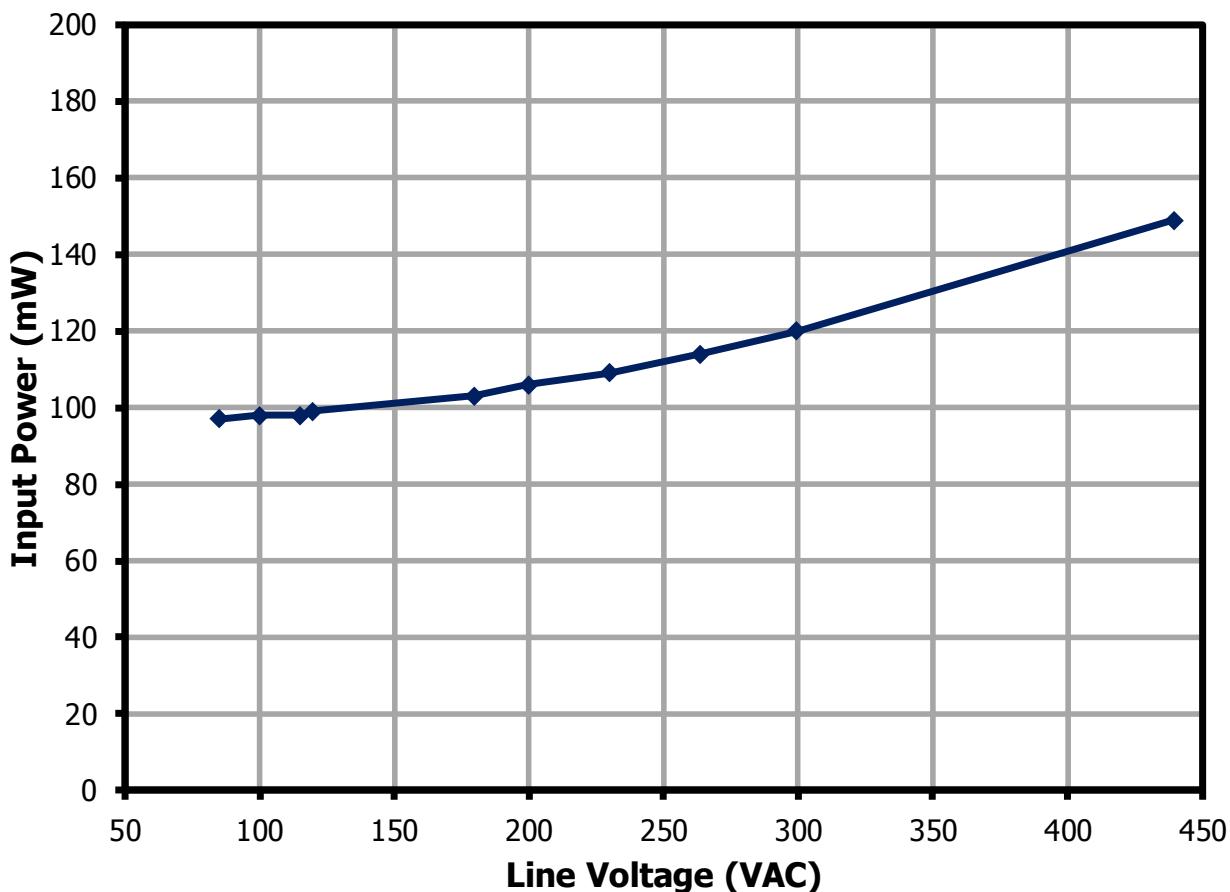


Figure 8 – No-Load Power vs. Input Line Voltage.

9.2 Efficiency

9.2.1 Efficiency vs Line

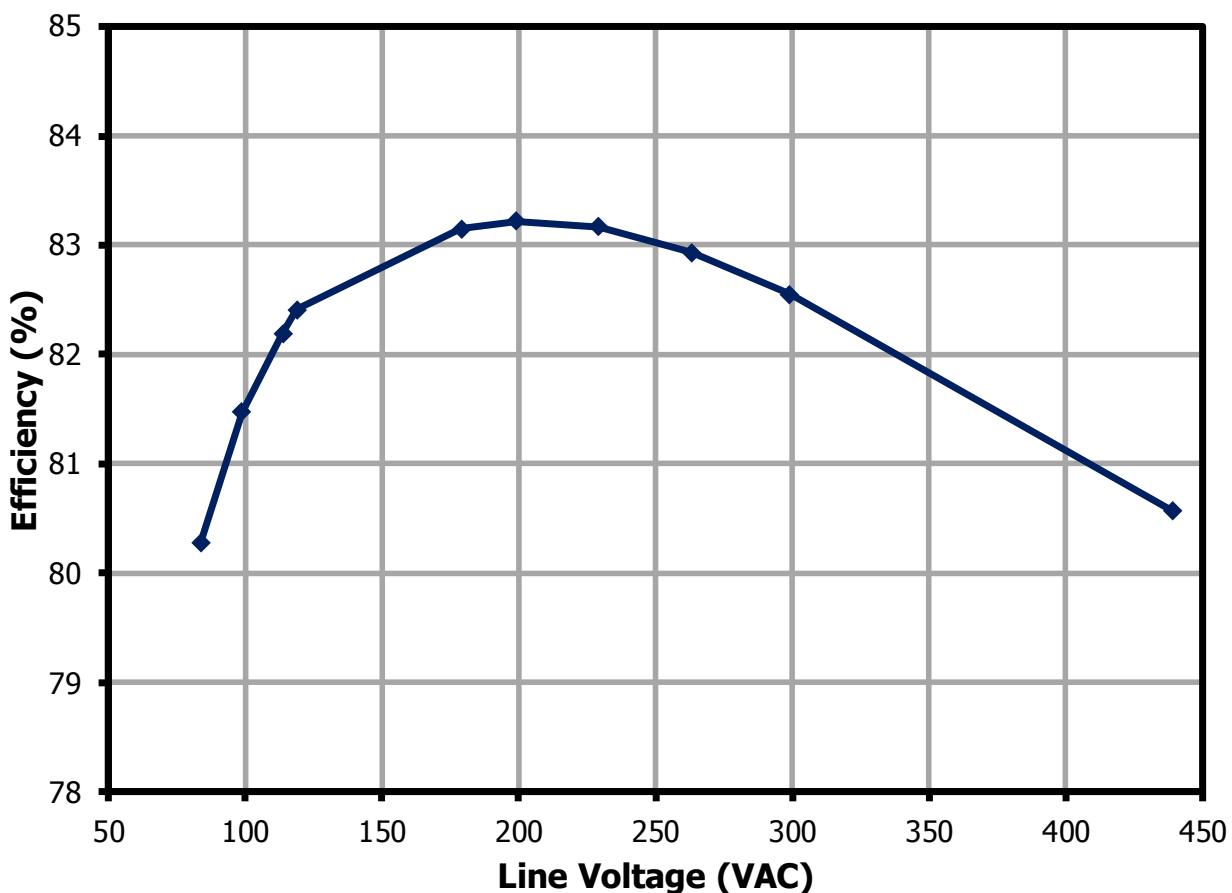


Figure 9 – Full Load Efficiency vs. Input Line Voltage.

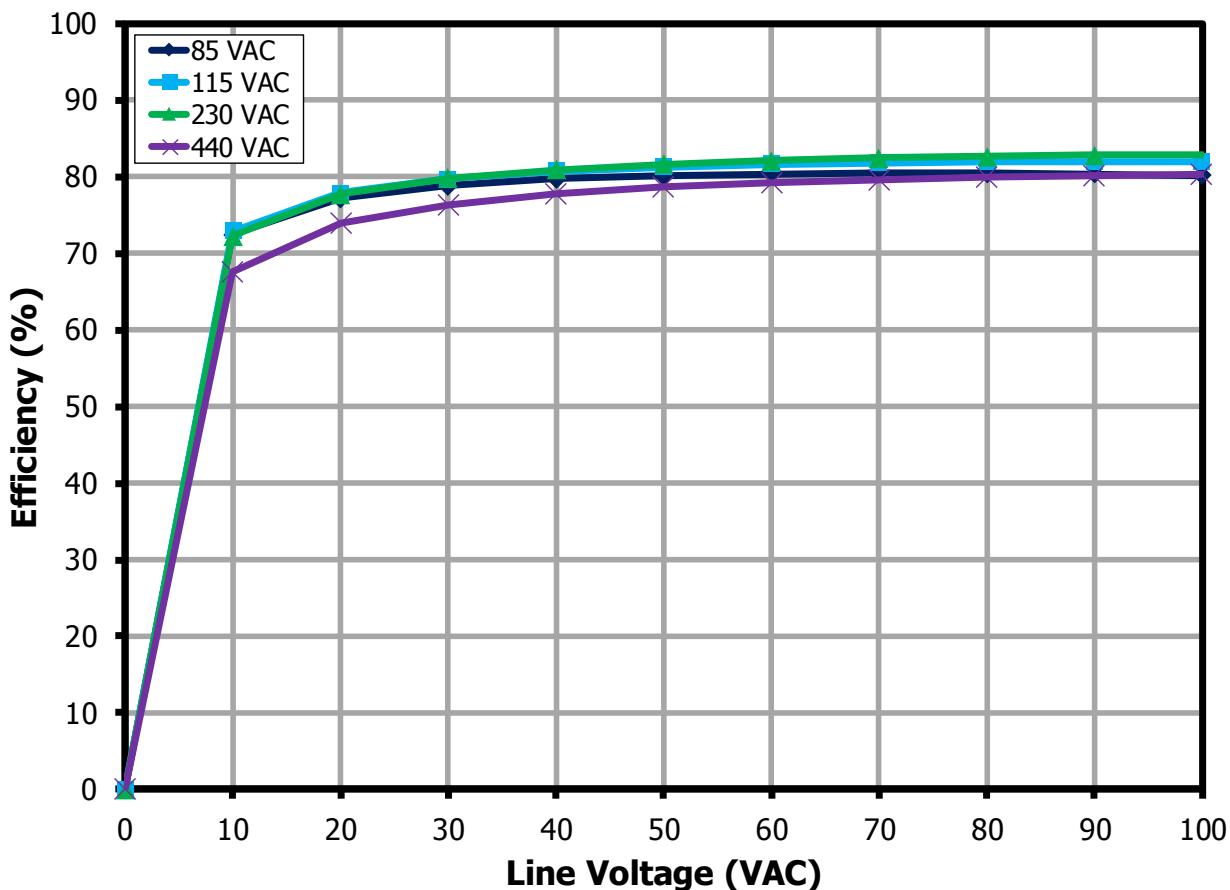
9.2.2 *Efficiency vs Load*

Figure 10 – Efficiency vs. Percent Load, at Different Input Line Voltages.

9.2.3 Average Efficiency

9.2.3.1 85 VAC Input

Input Measurement			Output 1 Measurement			Output 2 Measurement			Efficiency (%)
V _{IN} (RMS)	I _{IN} (mA)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	
83	163.1	8.71	12.01	500.0	6.01	4.94	198.1	0.98	80.2
84	124.1	6.52	12.02	375.0	4.51	4.95	148.0	0.73	80.4
84	85.8	4.36	12.04	249.9	3.01	4.95	98.2	0.49	80.1
84	46.8	2.23	12.06	145.0	1.51	4.95	48.2	0.24	78.2
Average Efficiency									79.7

9.2.3.2 115 VAC Input

Input Measurement			Output 1 Measurement			Output 2 Measurement			Efficiency (%)
V _{IN} (RMS)	I _{IN} (mA)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	
114	123.2	8.52	12.01	500.0	6.00	4.94	198.1	0.98	82.0
114	95.0	6.40	12.03	375.0	4.51	4.95	148.0	0.73	81.9
114	66.4	4.30	12.04	250.0	3.01	4.95	98.1	0.49	81.2
114	36.6	2.21	12.07	125.0	1.51	4.95	48.2	0.24	79.1
Average Efficiency									81.0

9.2.3.3 230 VAC Input

Input Measurement			Output 1 Measurement			Output 2 Measurement			Efficiency (%)
V _{IN} (RMS)	I _{IN} (mA)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	
229	72.1	8.43	12.03	500.0	6.02	4.94	198.0	0.98	83.0
229	56.1	6.36	12.04	375.0	4.52	4.94	148.1	0.73	82.5
229	39.5	4.29	12.06	249.9	3.01	4.95	98.1	0.49	81.6
230	22.0	2.21	12.08	125.0	1.51	4.95	48.2	0.24	78.9
Average Efficiency									81.5

9.2.3.4 440 VAC Input

Input Measurement			Output 1 Measurement			Output 2 Measurement			Efficiency (%)
V _{IN} (RMS)	I _{IN} (mA)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	
439	45.0	8.70	12.03	500.0	6.02	4.94	197.9	0.98	80.4
439	35.1	6.57	12.03	375.0	4.51	4.95	148.0	0.73	79.8
439	24.9	4.45	12.05	249.9	3.01	4.95	98.2	0.49	78.7
439	14.0	2.32	12.08	125.0	1.51	4.95	48.1	0.24	75.4
Average Efficiency									78.6

9.3 Output Voltage Regulation

9.3.1 5 V Load Regulation with Balanced Load

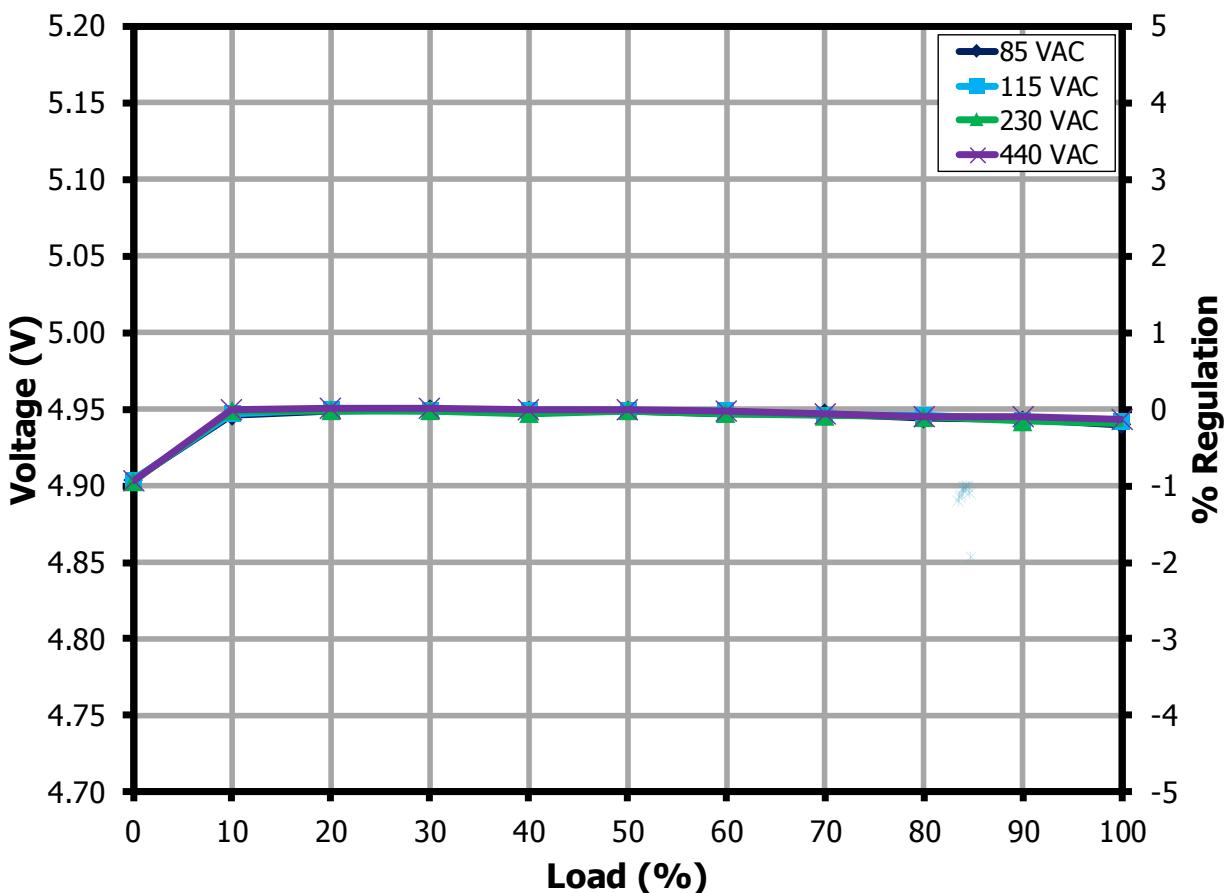


Figure 11 – 5 V Load Regulation.
Condition: Simultaneous Load Decrement.

9.3.2 12 V Load Regulation with Balanced Load

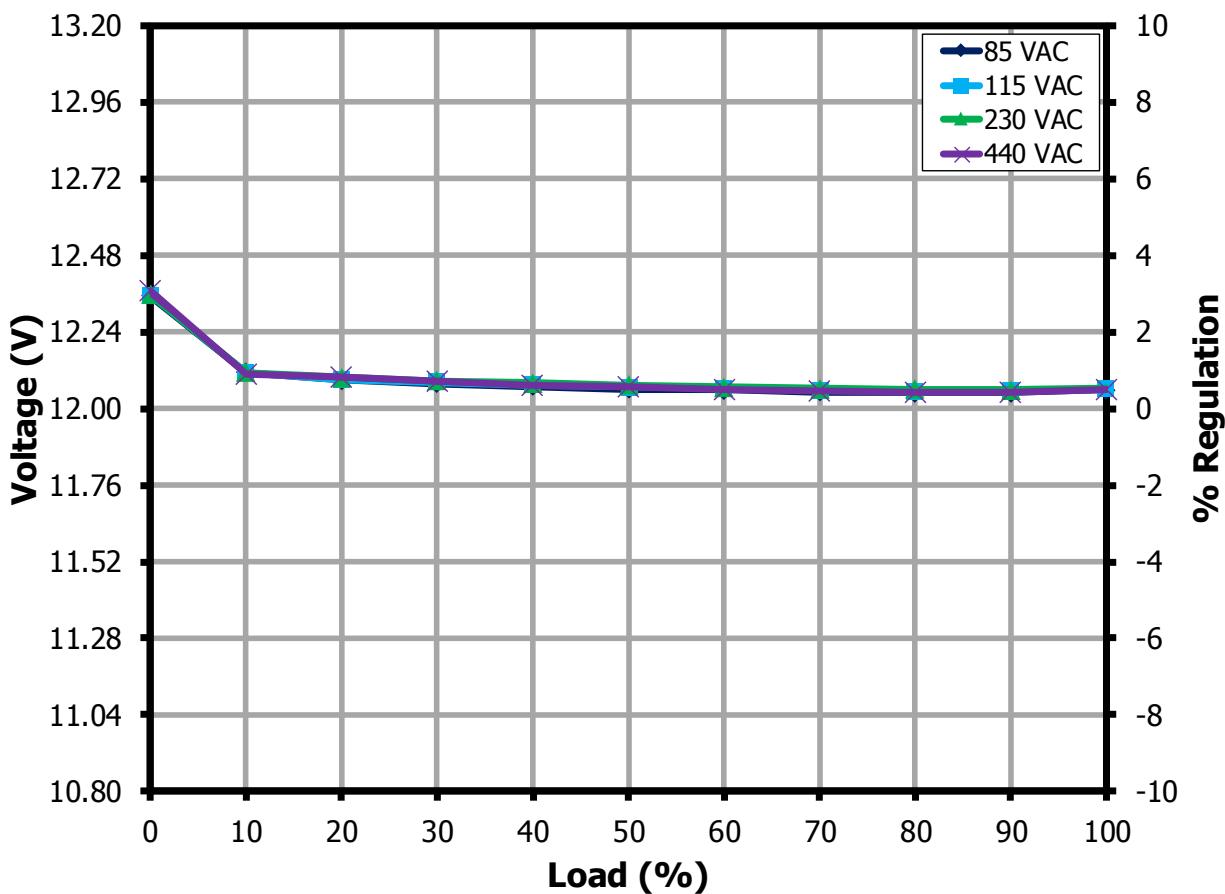


Figure 12 – 12 V Load Regulation.
Condition: Simultaneous Load Decrement.

9.3.3 5 V Load Regulation with Unbalanced Load

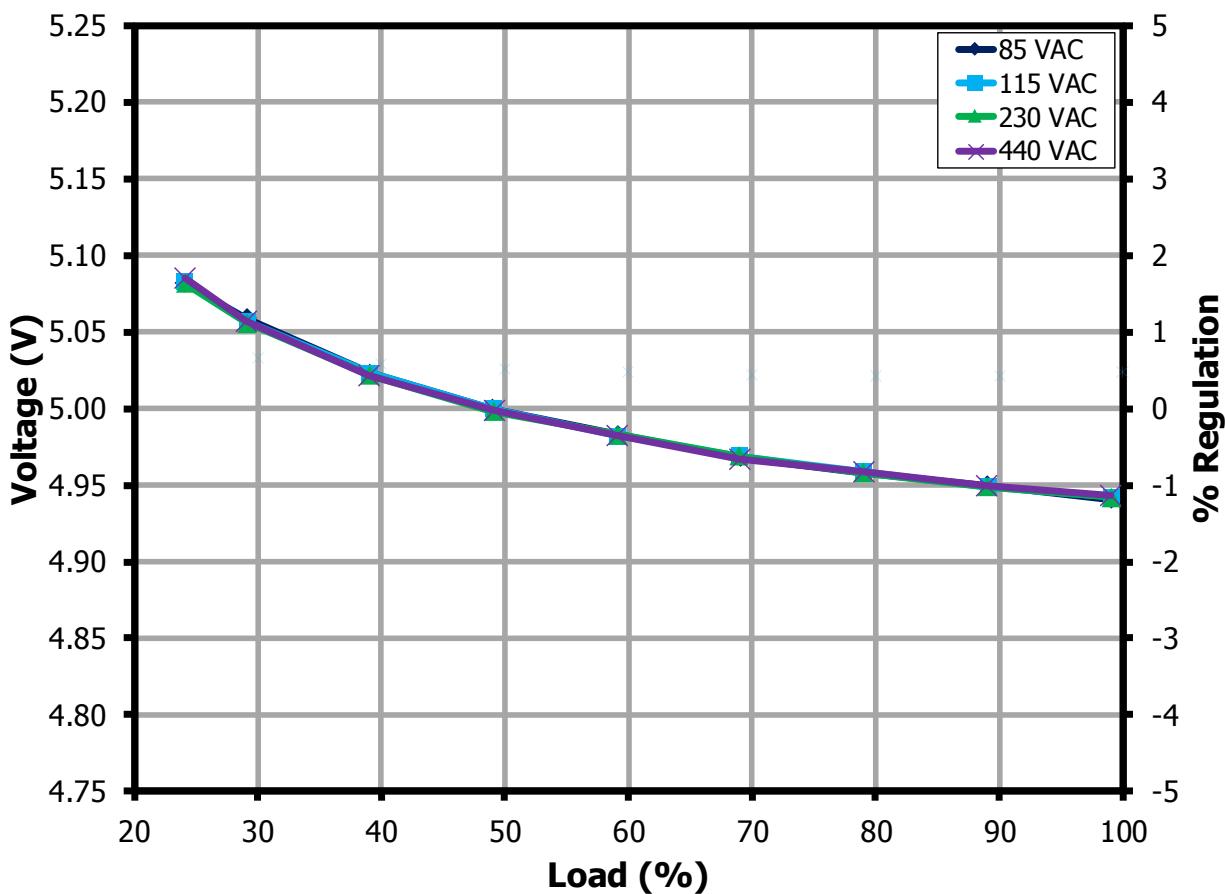


Figure 13 – 5 V Load Regulation.
Condition: 12 V at 500 mA, 5 V Load Sweep.

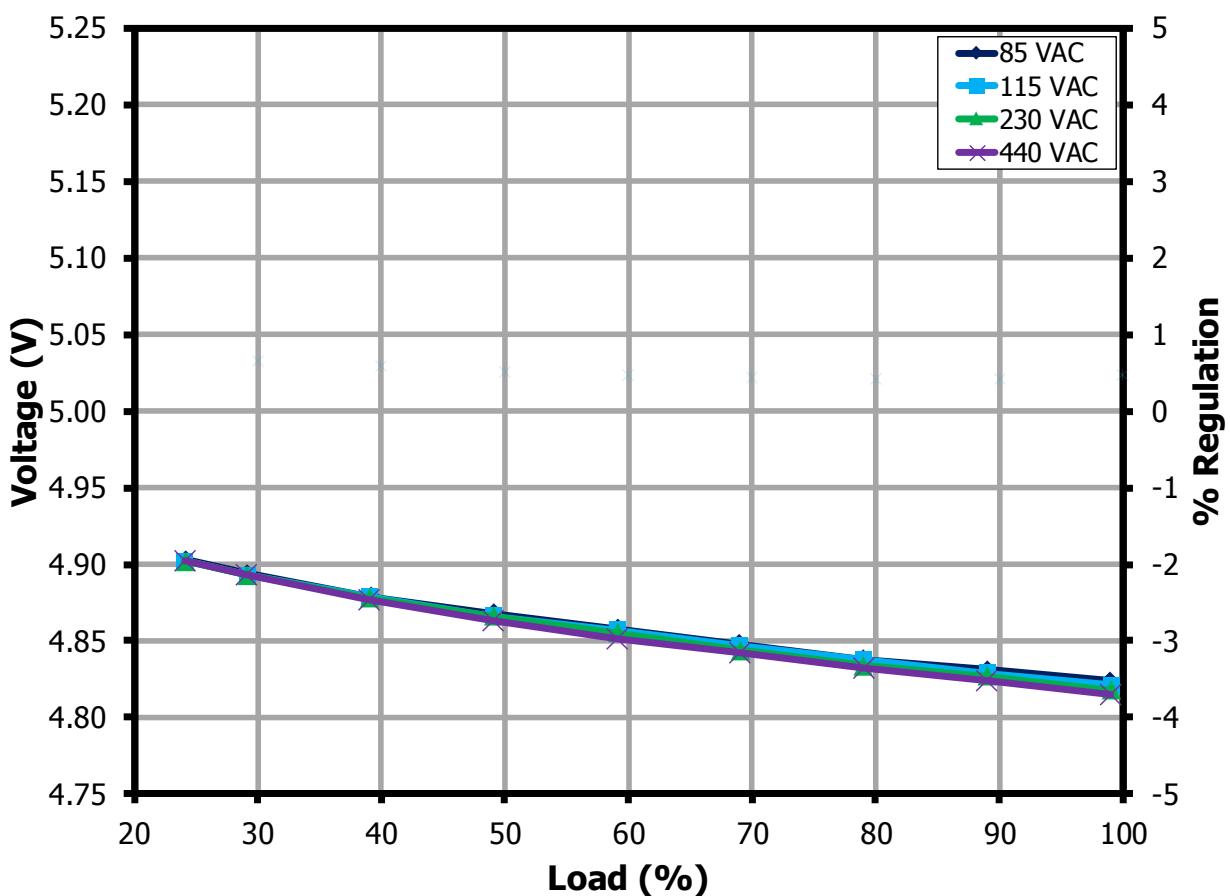


Figure 14 – 5 V Load Regulation.
Condition: 12 V at 50 mA, 5 V Load Sweep.

9.3.4 12 V Load Regulation with Unbalanced Load

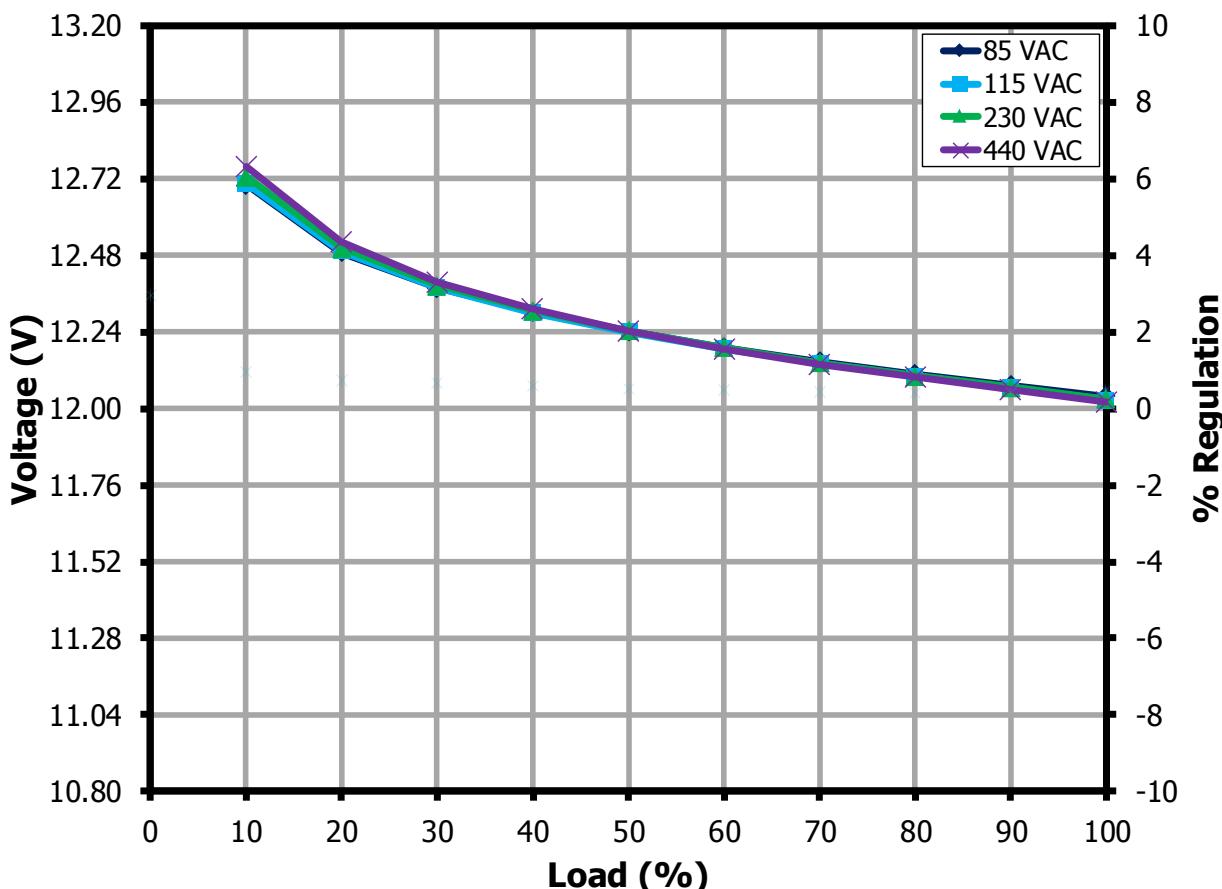


Figure 15 – 12 V Load Regulation.
Condition: 12 V Load Sweep, 5 V at 200 mA.

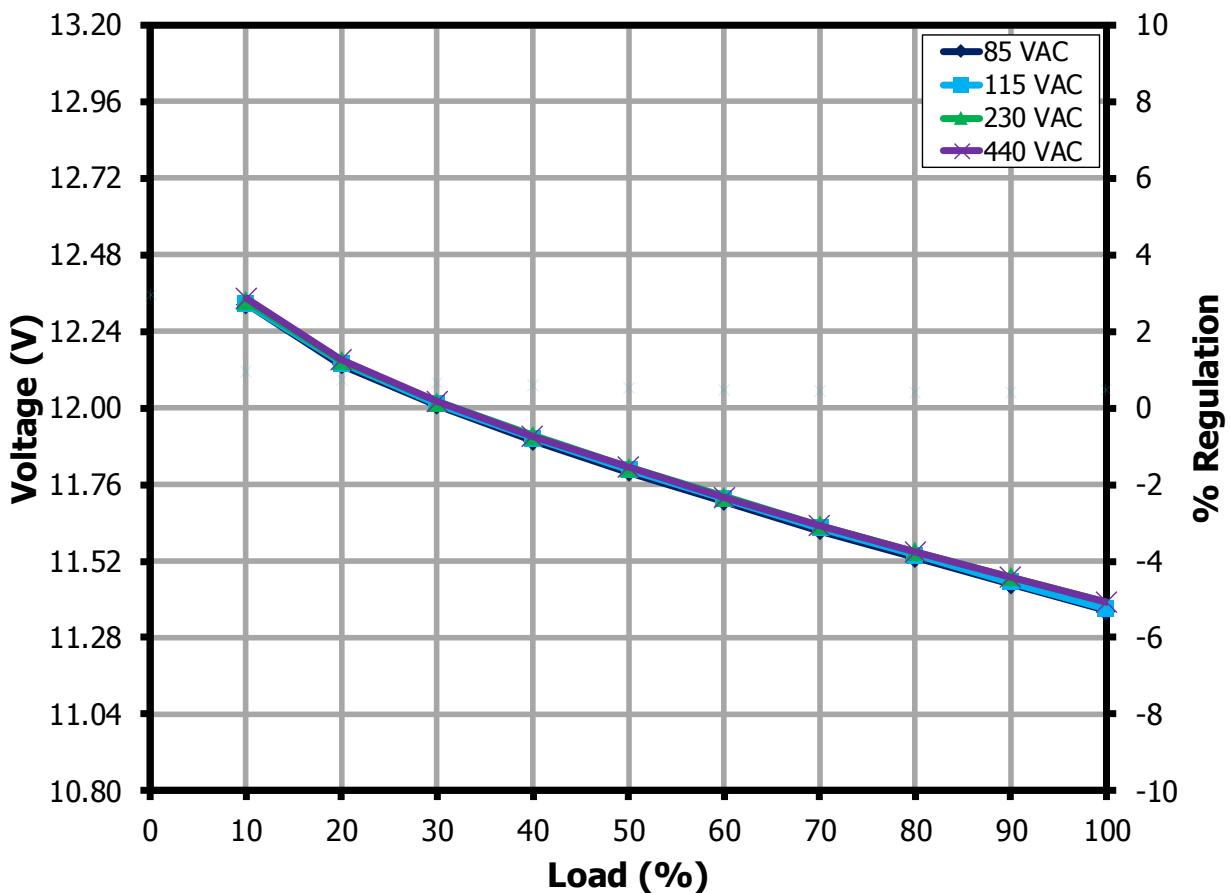


Figure 16 – 12 V Load Regulation.
Condition: 12 V Load Sweep, 5 V at 50 mA.

9.3.5 Line Regulation

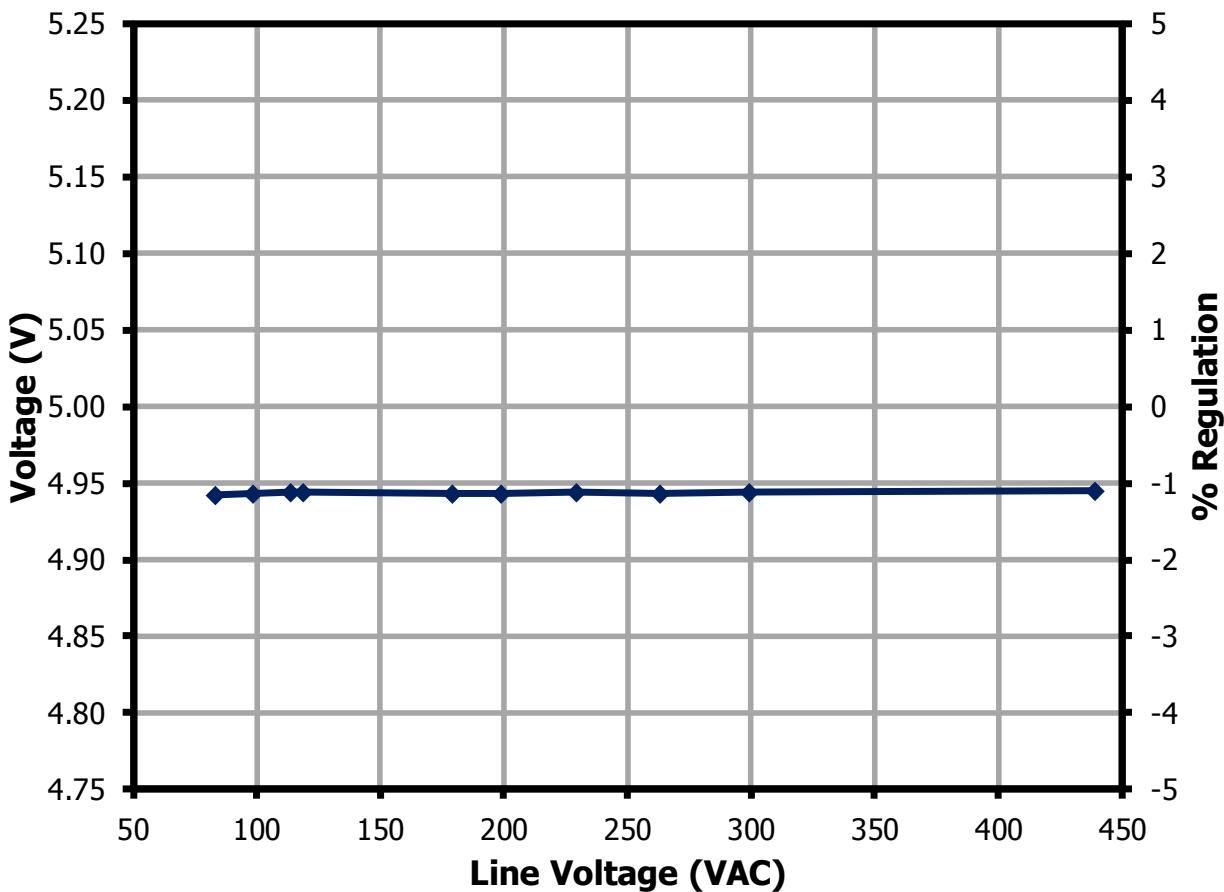


Figure 17 – 5 V Output Regulation vs. Input Line Voltage.

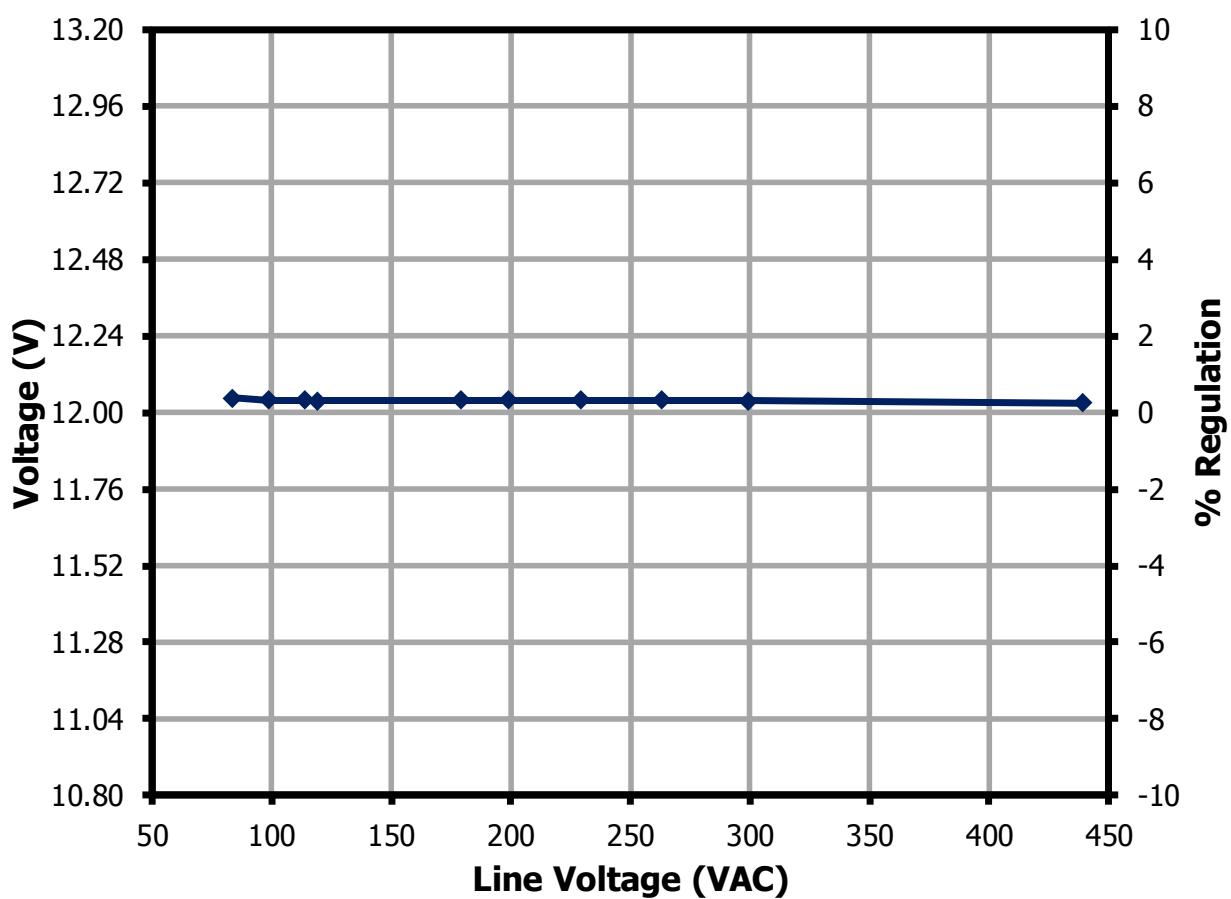


Figure 18 – 12 V Output Regulation vs. Input Line Voltage.

10 Waveforms

10.1 Output Voltage Ripple

10.1.1 Ripple Measurement Technique

For DC output ripple measurements, a modified oscilloscope test probe must be utilized in order to reduce spurious signals due to pick-up. Details of the probe modification are provided in the Figures below.

The 4987BA probe adapter is affixed with two capacitors tied in parallel across the probe tip. The capacitors include one (1) 0.1 μF / 50 V ceramic type and one (1) 47 μF / 50 V aluminum electrolytic. The aluminum electrolytic type capacitor is polarized, so proper polarity across DC outputs must be maintained (see below). Ripple measurement done at the end of a 100 m Ω cable.



Figure 19 – Oscilloscope Probe Prepared for Ripple Measurement. (End Cap and Ground Lead Removed.)

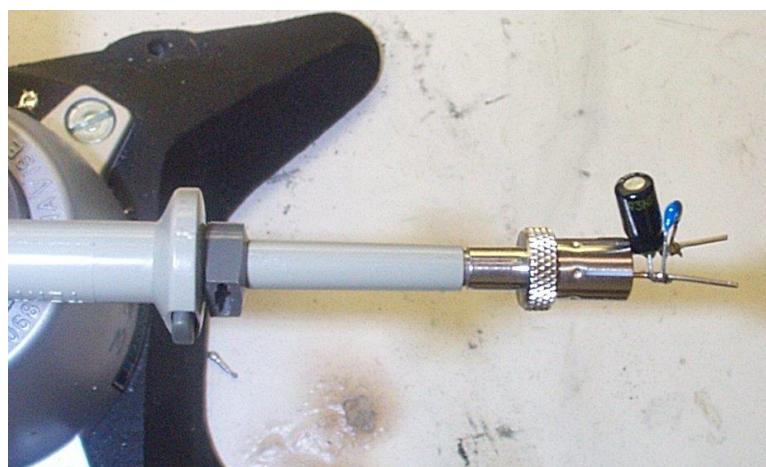


Figure 20 – Oscilloscope Probe with Probe Master (www.probemaster.com) 4987A BNC Adapter. (Modified with wires for ripple measurement, and two parallel decoupling capacitors added.)

10.1.2 Ripple Waveforms at Full Load

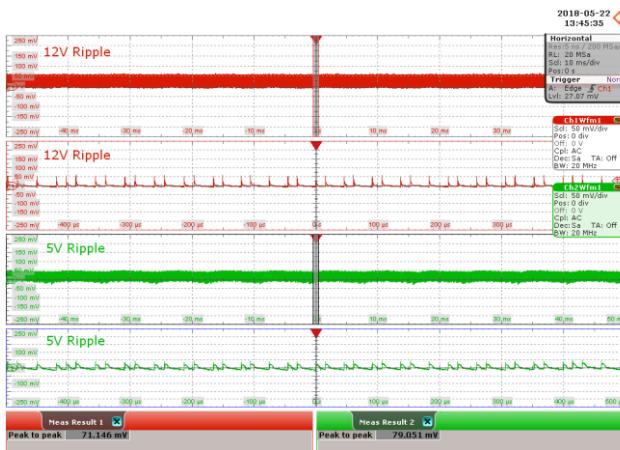


Figure 21 – 85 VAC Input.

Vertical: 50 mV / div.
Horizontal: 10 ms / div., 100 μ s / div.
12 V Ripple: 71.146 mV_{PK-PK}.
5 V Ripple: 79.051 mV_{PK-PK}.

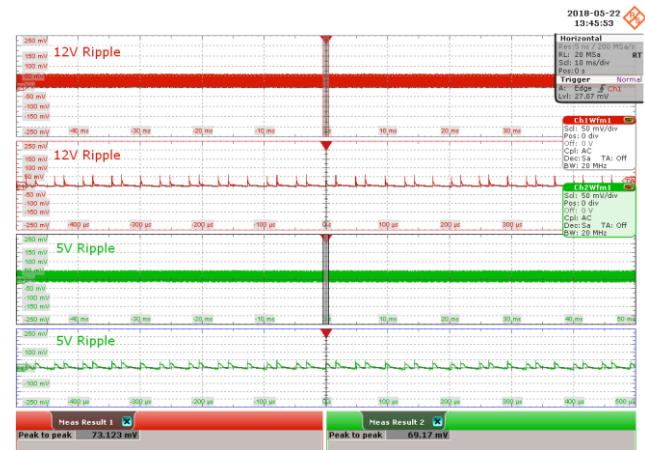


Figure 22 – 115 VAC Input.

Vertical: 50 mV / div.
Horizontal: 10 ms / div., 100 μ s / div.
12 V Ripple: 73.123 mV_{PK-PK}.
5 V Ripple: 69.170 mV_{PK-PK}.

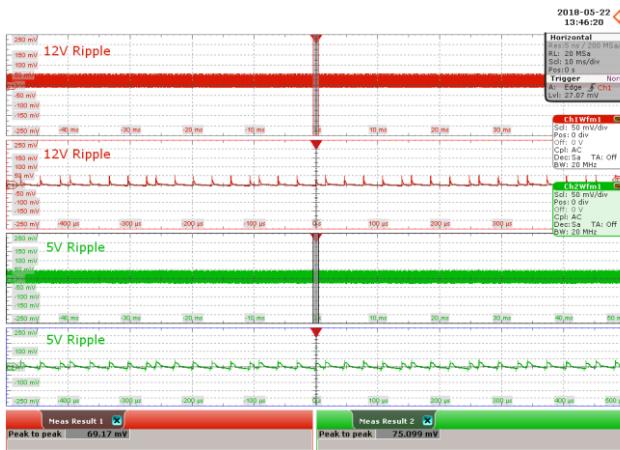


Figure 23 – 230 VAC Input.

Vertical: 50 mV / div.
Horizontal: 10 ms / div., 100 μ s / div.
12 V Ripple: 69.170 mV_{PK-PK}.
5 V Ripple: 75.099 mV_{PK-PK}.

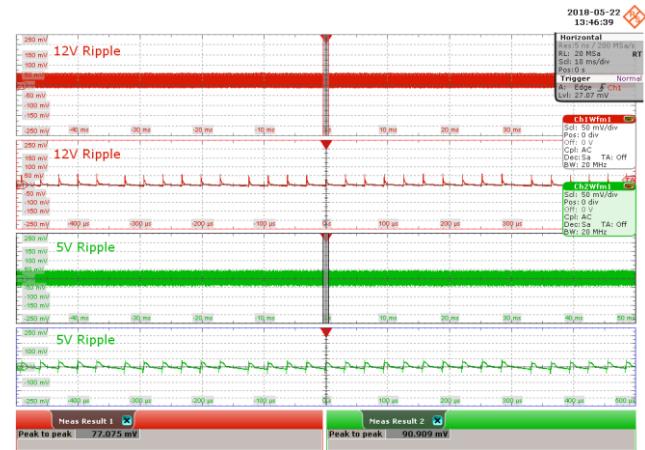
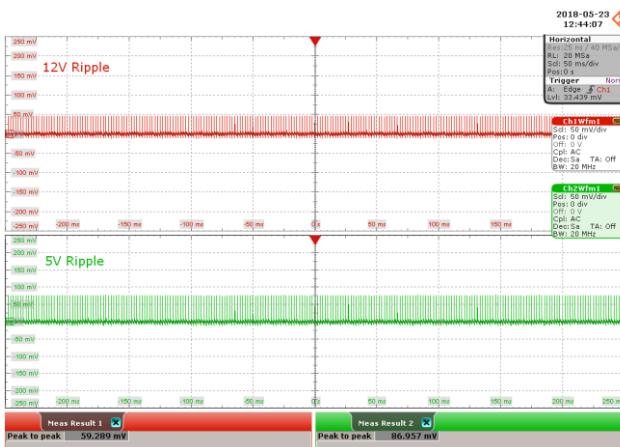


Figure 24 – 440 VAC Input.

Vertical: 50 mV / div.
Horizontal: 10 ms / div., 100 μ s / div.
12 V Ripple: 77.075 mV_{PK-PK}.
5 V Ripple: 90.909 mV_{PK-PK}.

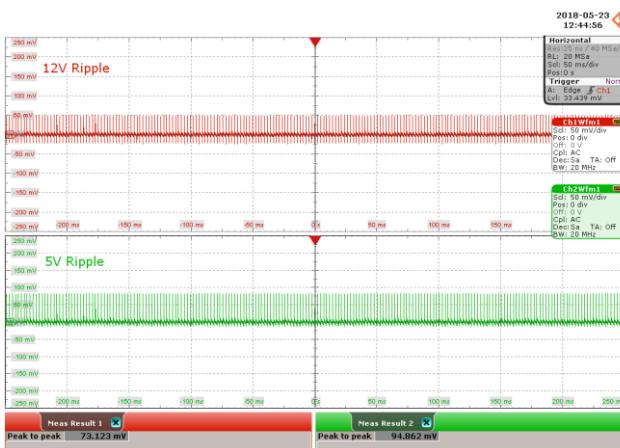
10.1.3 Ripple Waveforms at No-Load

**Figure 25 – 85 VAC Input.**

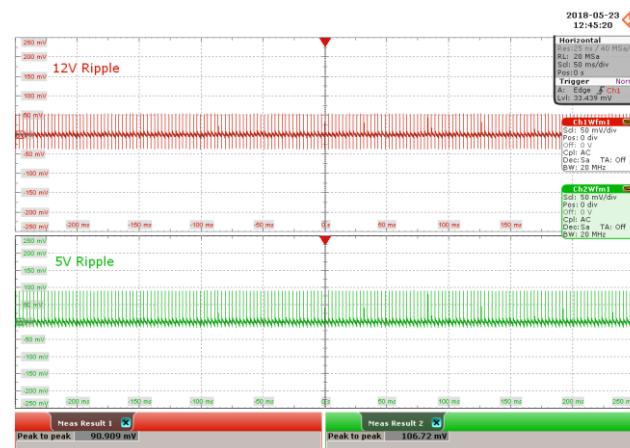
Vertical: 50 mV / div.
Horizontal: 50 ms / div.
12 V Ripple: 59.289 mV_{PK-PK}.
5 V Ripple: 86.957 mV_{PK-PK}.

**Figure 26 – 115 VAC Input.**

Vertical: 50 mV / div.
Horizontal: 50 ms / div.
12 V Ripple: 61.265 mV_{PK-PK}.
5 V Ripple: 88.933 mV_{PK-PK}.

**Figure 27 – 230 VAC Input.**

Vertical: 50 mV / div.
Horizontal: 50 ms / div.
12 V Ripple: 73.123 mV_{PK-PK}.
5 V Ripple: 94.862 mV_{PK-PK}.

**Figure 28 – 440 VAC Input.**

Vertical: 50 mV / div.
Horizontal: 50 ms / div.
12 V Ripple: 90.909 mV_{PK-PK}.
5 V Ripple: 106.72 mV_{PK-PK}.



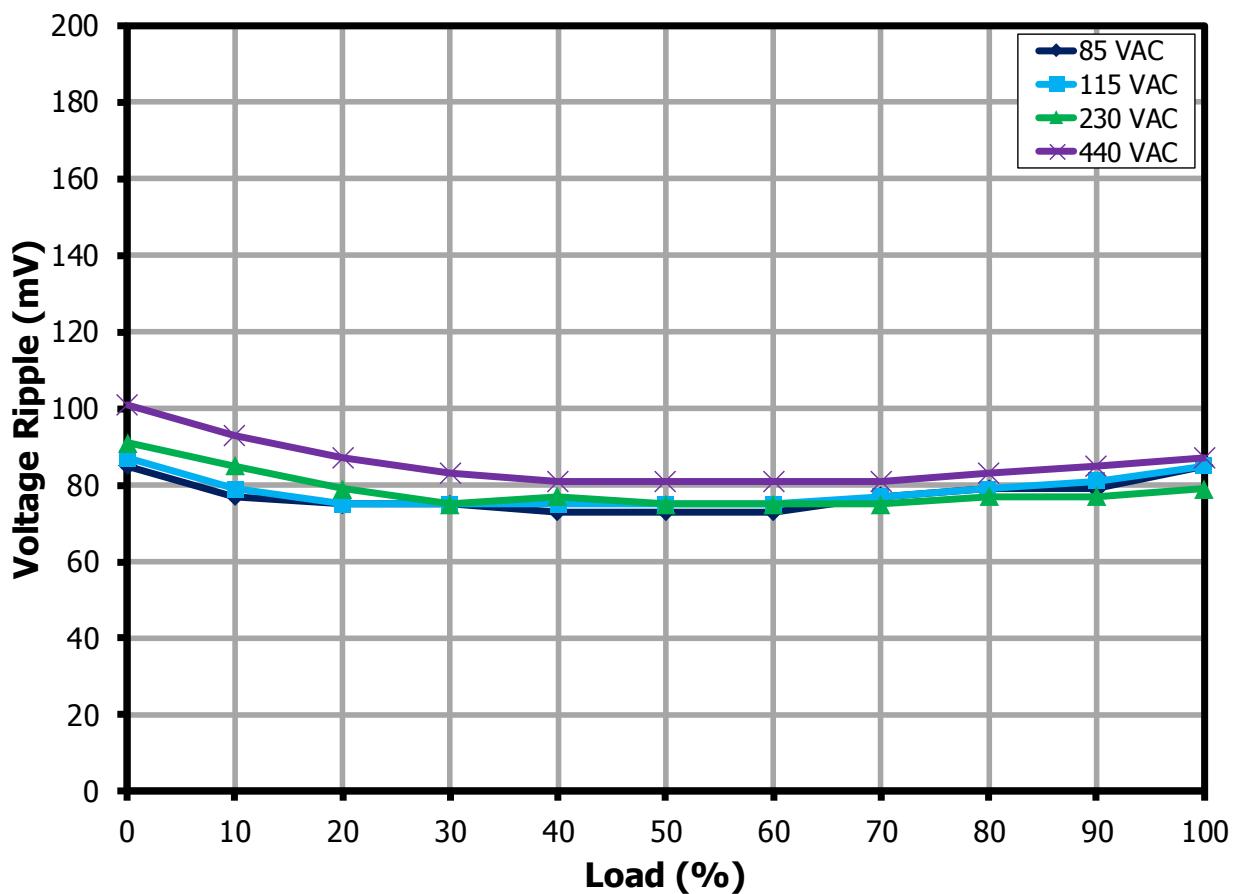
10.1.4 *Ripple vs. Load*

Figure 29 – 5 V Output Ripple vs. Percent Load.

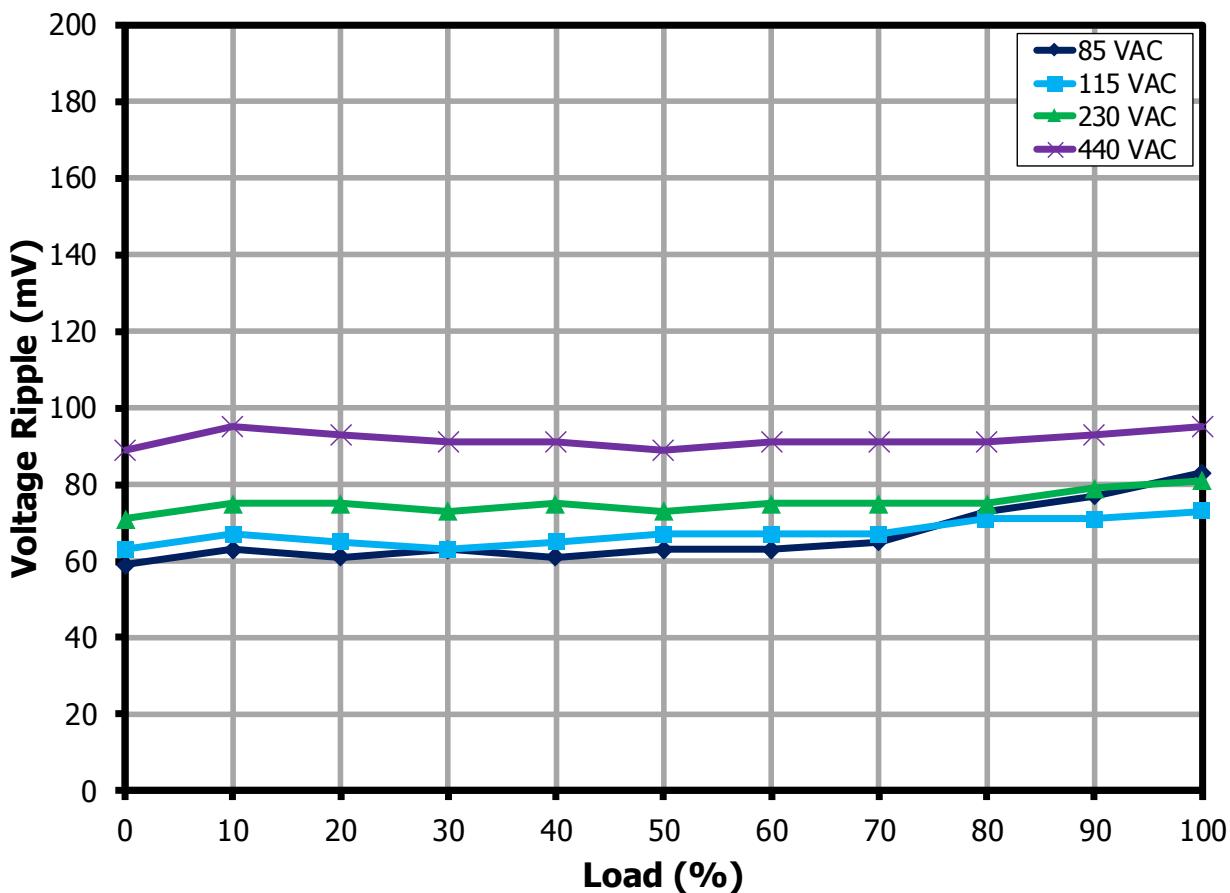


Figure 30 – 12 V Output Ripple vs. Percent Load.

10.2 Switching Waveforms

10.2.1 V_{DS} and I_{DS}

Test conditions: 12 V load set to CC at 500 mA, 5 V load set to CC at 200 mA



Figure 31 – 85 VAC Input.

Upper: V_{DS} , 200 V / div., 10 μ s / div.
Lower: I_{DS} , 100 mA / div.

$V_{DS(\text{MAX})}$: 267.98 V.
 $I_{DS(\text{MAX})}$: 493.68 mA.

Figure 32 – 115 VAC Input.

Upper: V_{DS} , 200 V / div., 10 μ s / div.
Lower: I_{DS} , 100 mA / div.

$V_{DS(\text{MAX})}$: 307.51 V.
 $I_{DS(\text{MAX})}$: 501.58 mA.

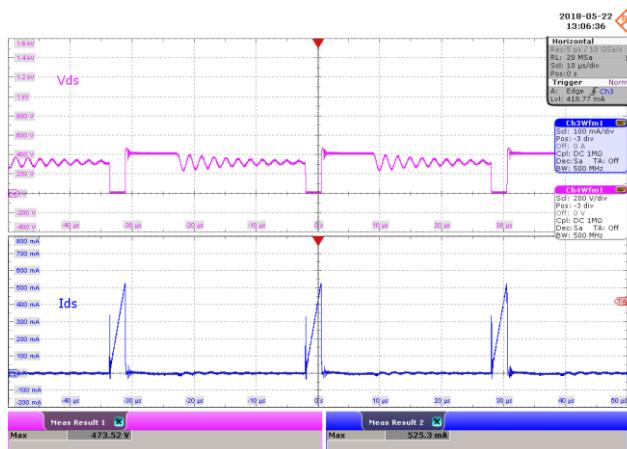


Figure 33 – 230 VAC Input.

Upper: V_{DS} , 200 V / div., 10 μ s / div.
Lower: I_{DS} , 100 mA / div.

$V_{DS(\text{MAX})}$: 473.52 V.
 $I_{DS(\text{MAX})}$: 523.30 mA.

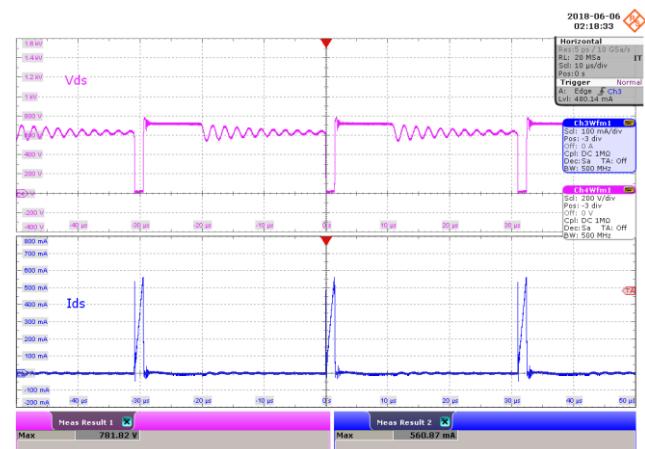


Figure 34 – 450 VAC Input.

Upper: V_{DS} , 200 V / div., 10 μ s / div.
Lower: I_{DS} , 100 mA / div.

$V_{DS(\text{MAX})}$: 781.82 V.
 $I_{DS(\text{MAX})}$: 560.87 mA.

10.2.2 5 V Output Diode Voltage and Current

Test conditions: 12 V load set to CC at 500 mA, 5 V load set to CC at 200 mA

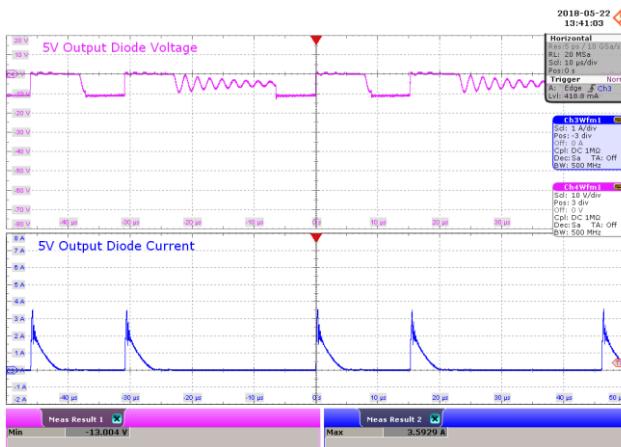


Figure 35 – 85 VAC Input.

Upper: PIV, 10 V / div., 10 μ s / div.
Lower: $I_{D(MAX)}$, 1 A / div.
PIV: 13.004 V.
 $I_{D(MAX)}$: 3.5929 A.

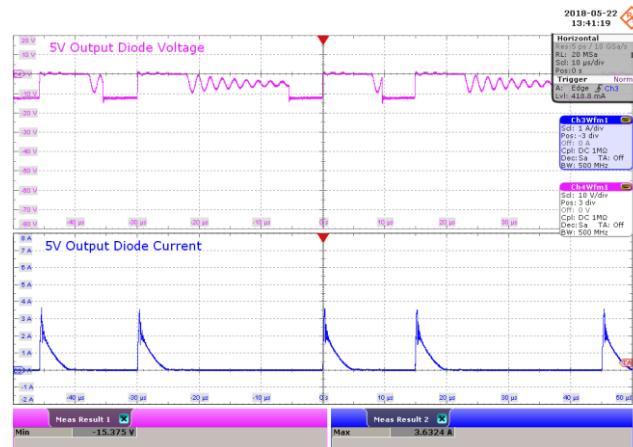


Figure 36 – 115 VAC Input.

Upper: PIV, 10 V / div., 10 μ s / div.
Lower: $I_{D(MAX)}$, 1 A / div.
PIV: 15.375 V.
 $I_{D(MAX)}$: 3.6324 A.

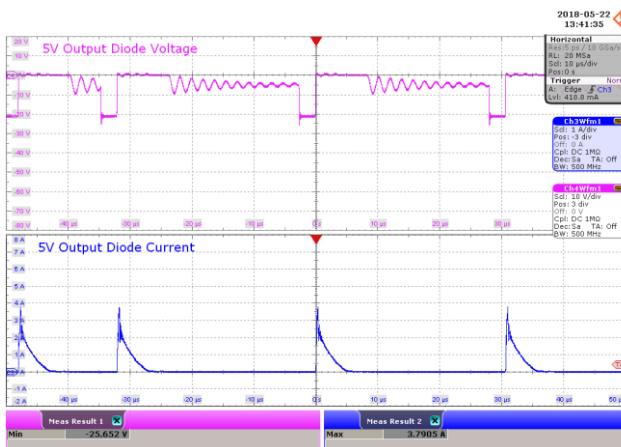


Figure 37 – 230 VAC Input.

Upper: PIV, 10 V / div., 10 μ s / div.
Lower: $I_{D(MAX)}$, 1 A / div.
PIV: 25.652 V.
 $I_{D(MAX)}$: 3.7905 A.

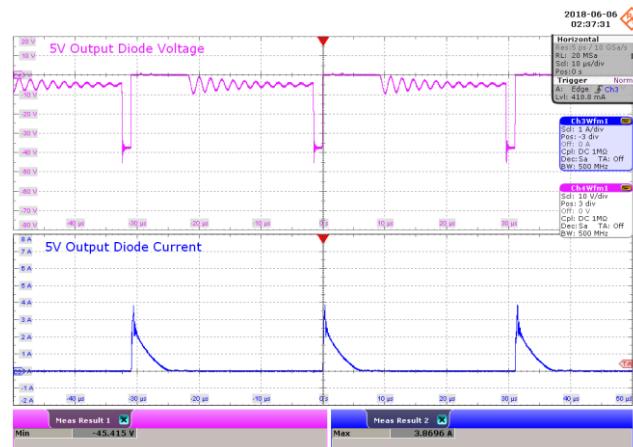


Figure 38 – 450 VAC Input.

Upper: PIV, 10 V / div., 10 μ s / div.
Lower: $I_{D(MAX)}$, 1 A / div.
PIV: 45.415 V.
 $I_{D(MAX)}$: 3.9091 A.



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10.2.3 12 V Output Diode Voltage and Current

Test conditions: 12 V load set to CC at 500 mA, 5 V load set to CC at 200 mA

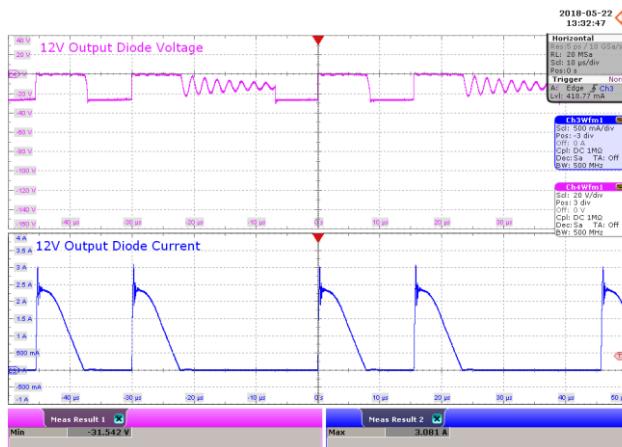


Figure 39 – 85 VAC Input.

Upper: PIV, 20 V / div., 10 μ s / div.
Lower: $I_{D(\text{MAX})}$, 500 mA / div.
PIV: 31.542 V.
 $I_{D(\text{MAX})}$: 3.0810 A.

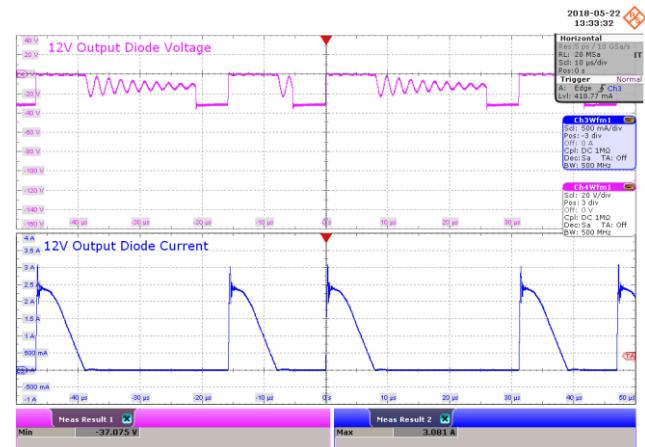


Figure 40 – 115 VAC Input.

Upper: PIV, 20 V / div., 10 μ s / div.
Lower: $I_{D(\text{MAX})}$, 500 mA / div.
PIV: 37.075 V.
 $I_{D(\text{MAX})}$: 3.0810 A.

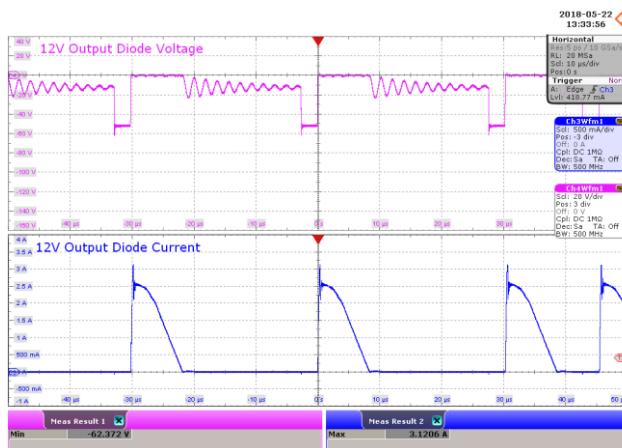


Figure 41 – 230 VAC Input.

Upper: PIV, 20 V / div., 10 μ s / div.
Lower: $I_{D(\text{MAX})}$, 500 mA / div.
PIV: 62.372 V.
 $I_{D(\text{MAX})}$: 3.1206 A.

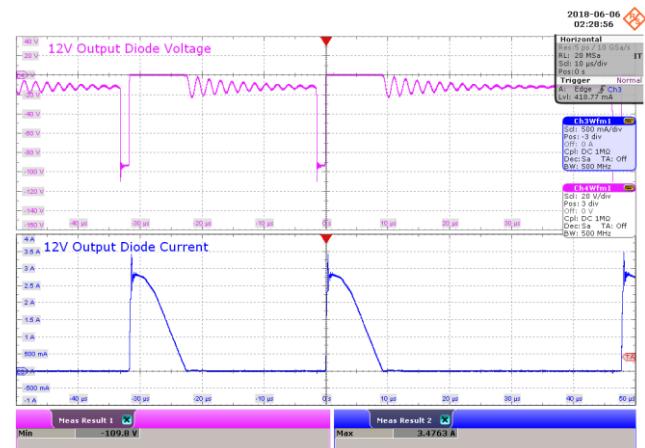


Figure 42 – 450 VAC Input.

Upper: PIV, 20 V / div., 10 μ s / div.
Lower: $I_{D(\text{MAX})}$, 500 mA / div.
PIV: 109.80 V.
 $I_{D(\text{MAX})}$: 3.4763 A.

10.3 Start-up Performance

10.3.1 12 V Start-up Operation V_{IN} , V_{OUT} and I_{OUT}

Test conditions: 12 V load set to CR at $24\ \Omega$, 5 V load set to CR at $25\ \Omega$

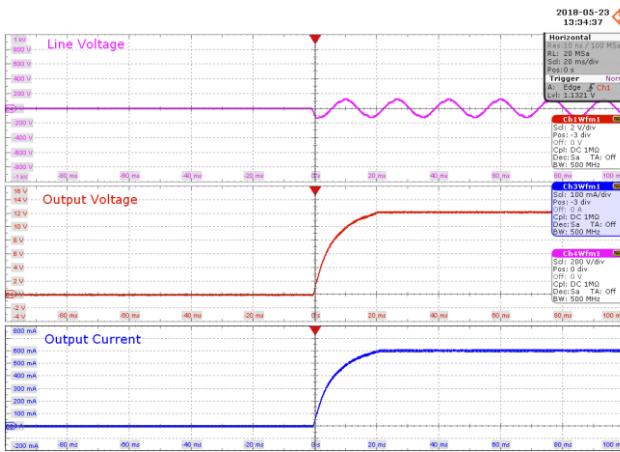


Figure 43 – 85 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 2 V / div.
Lower: I_{OUT} , 100 mA / div.

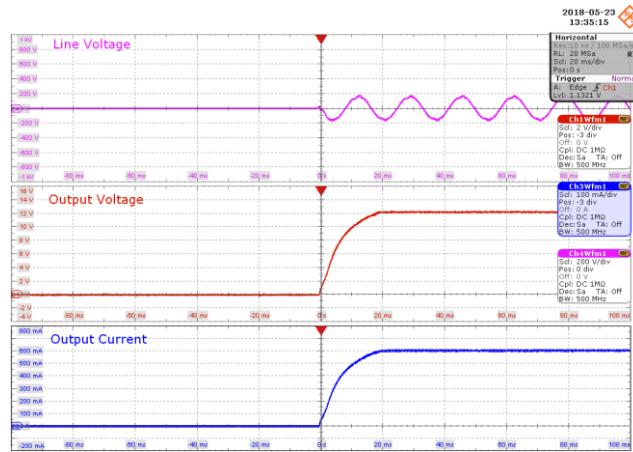


Figure 44 – 115 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 2 V / div.
Lower: I_{OUT} , 100 mA / div.

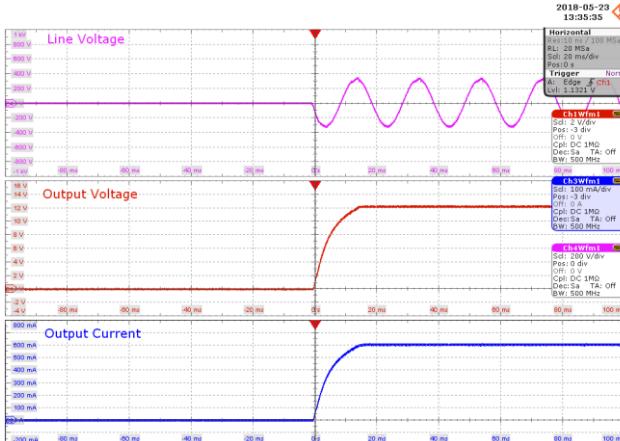


Figure 45 – 230 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 2 V / div.
Lower: I_{OUT} , 100 mA / div.

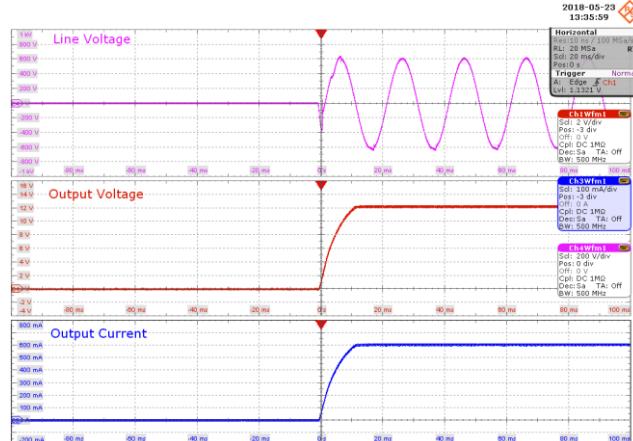


Figure 46 – 440 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 2 V / div.
Lower: I_{OUT} , 100 mA / div.



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10.3.2 5 V Start-up Operation V_{IN} , V_{OUT} and I_{OUT}

Test conditions: 12 V load set to CR at 24Ω , 5 V load set to CR at 25Ω

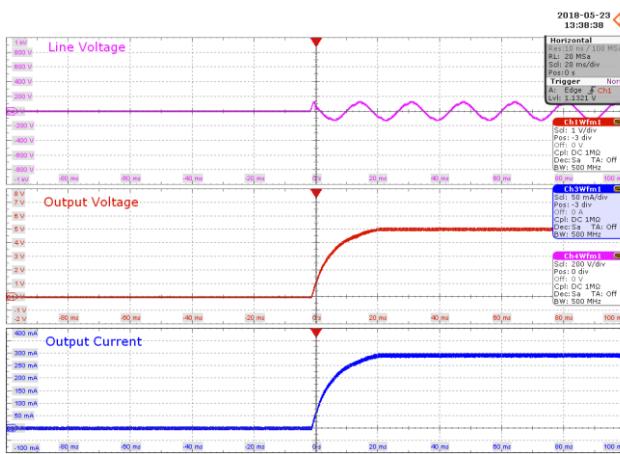


Figure 47 – 85 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 1 V / div.
Lower: I_{OUT} , 50 mA / div.

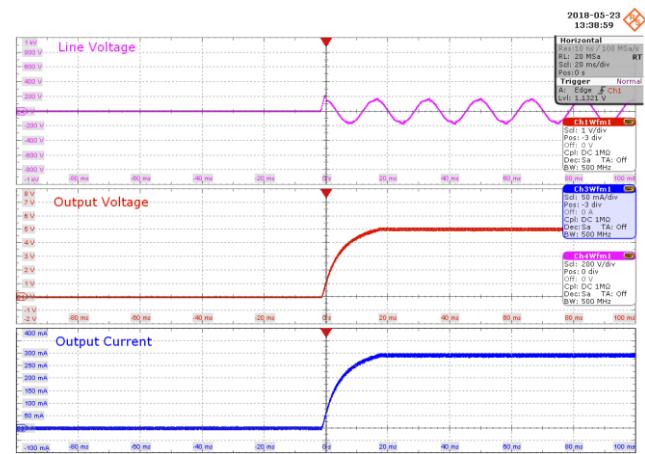


Figure 48 – 115 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 1 V / div.
Lower: I_{OUT} , 50 mA / div.

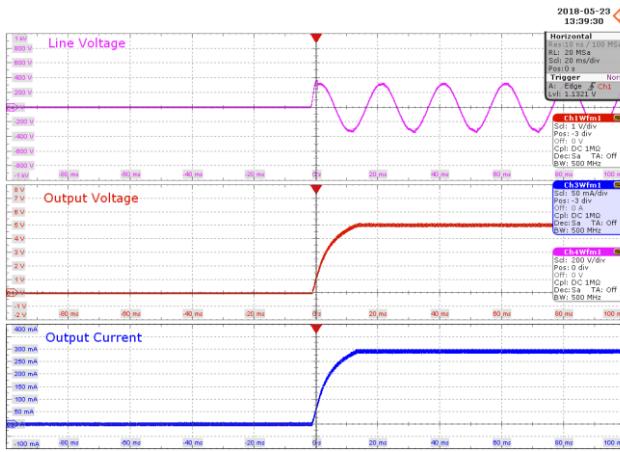


Figure 49 – 230 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 1 V / div.
Lower: I_{OUT} , 50 mA / div.

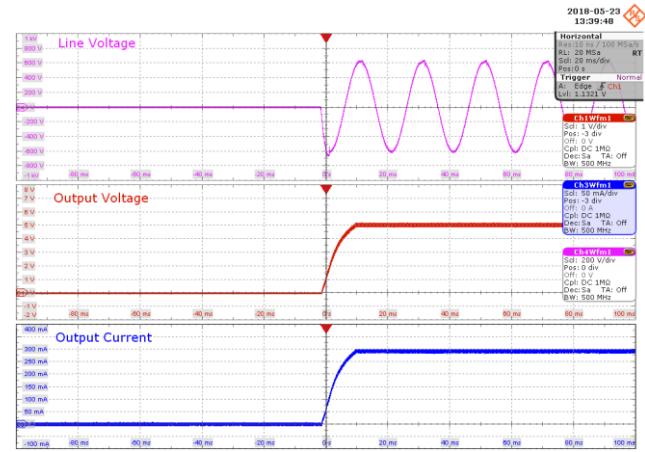


Figure 50 – 440 VAC Input.

Upper: V_{IN} , 200 V / div., 20 ms / div.
Middle: V_{OUT} , 1 V / div.
Lower: I_{OUT} , 50 mA / div.

10.3.3 Start-up Operation V_{DS} and I_{DS}

Test conditions: 12 V load set to CC at 500 mA, 5 V load set to CC at 200 mA



Figure 51 – 85 VAC Input.

Upper: V_{DS} , 200 V / div., 2 ms / div.
Lower: I_{DS} , 200 mA / div.
Zoom: 200 μ s / div.
 $V_{DS(\text{MAX})}$: 283.79 V.
 $I_{DS(\text{MAX})}$: 560.47 mA.

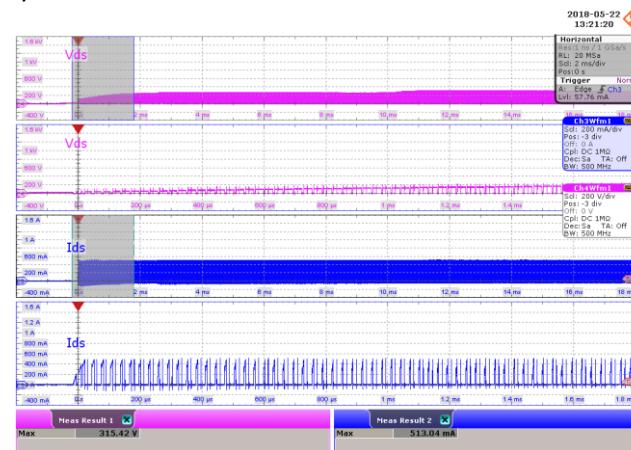


Figure 52 – 115 VAC Input.

Upper: V_{DS} , 200 V / div., 2 ms / div.
Lower: I_{DS} , 200 mA / div.
Zoom: 200 μ s / div.
 $V_{DS(\text{MAX})}$: 315.42 V.
 $I_{DS(\text{MAX})}$: 513.04 mA.

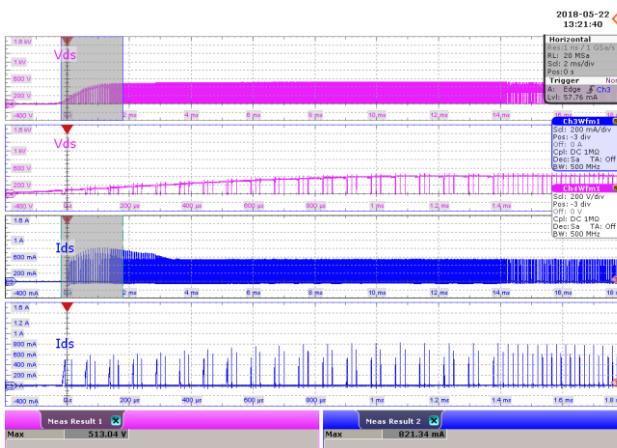


Figure 53 – 85 VAC Input.

Upper: V_{DS} , 200 V / div., 2 ms / div.
Lower: I_{DS} , 200 mA / div.
Zoom: 200 μ s / div.
 $V_{DS(\text{MAX})}$: 513.04 V.
 $I_{DS(\text{MAX})}$: 821.34 mA.

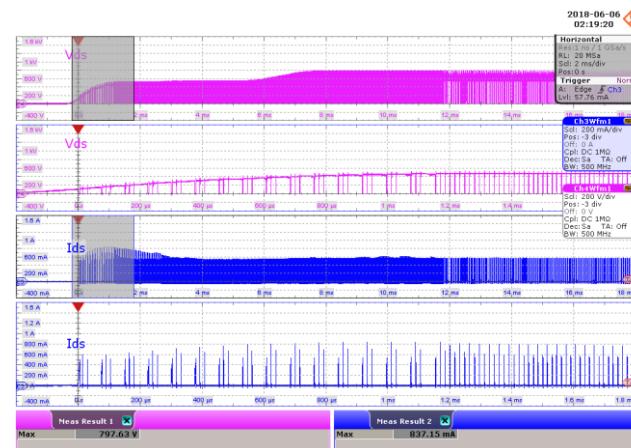


Figure 54 – 450 VAC Input.

Upper: V_{DS} , 200 V / div., 10 μ s / div.
Lower: I_{DS} , 100 mA / div.
 $V_{DS(\text{MAX})}$: 797.63 V.
 $I_{DS(\text{MAX})}$: 837.15 mA.



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10.4 Output Load Transient

10.4.1 5 V Output Transient

Test conditions: 5 V load swings from 50 mA to full load, 12 V at full load

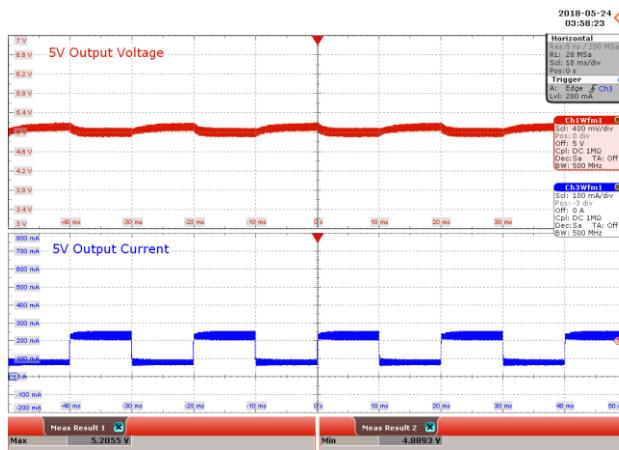


Figure 55 – 85 VAC Input.

Upper: 5 V V_{OUT} , 400 mV / div., 10 ms / div.
Lower: 5 V I_{OUT} , 100 mA / div.

V_{MAX} : 5.2055 V.

V_{MIN} : 4.8893 V.

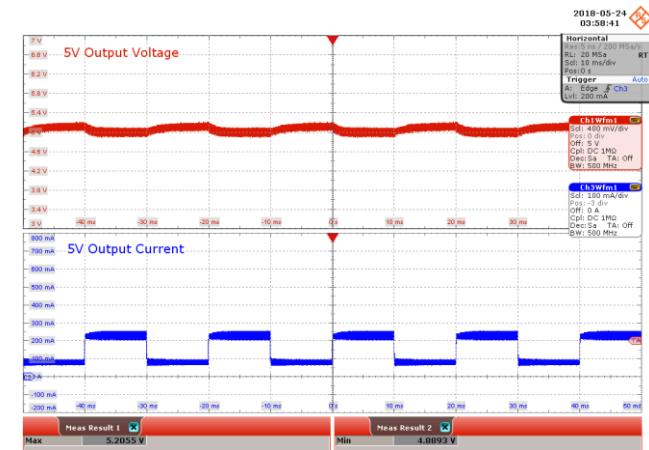


Figure 56 – 115 VAC Input.

Upper: 5 V V_{OUT} , 400 mV / div., 10 ms / div.
Lower: 5 V I_{OUT} , 100 mA / div.

V_{MAX} : 5.2055 V.

V_{MIN} : 4.8893 V.

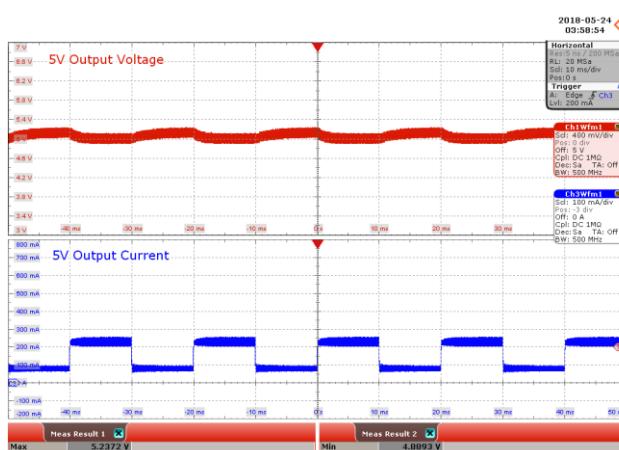


Figure 57 – 230 VAC Input.

Upper: 5 V V_{OUT} , 400 mV / div., 10 ms / div.
Lower: 5 V I_{OUT} , 100 mA / div.

V_{MAX} : 5.2372 V.

V_{MIN} : 4.8893 V.

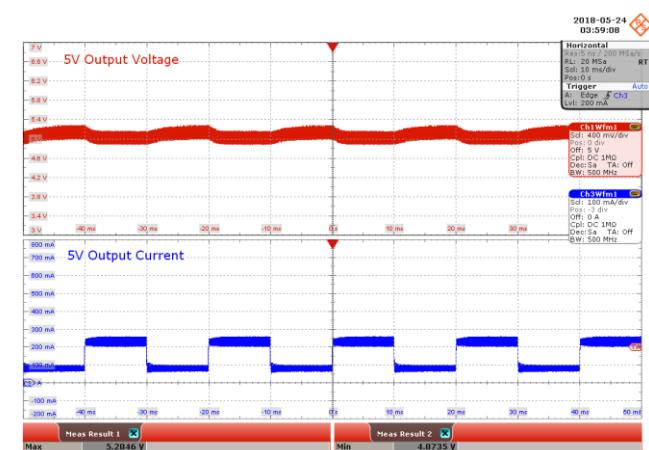


Figure 58 – 440 VAC Input.

Upper: 5 V V_{OUT} , 400 mV / div., 10 ms / div.
Lower: 5 V I_{OUT} , 100 mA / div.

V_{MAX} : 5.2846 V.

V_{MIN} : 4.8735 V.

10.4.2 12 V Output Transient

Test conditions: 12 V load swings from 50 mA to full load, 5 V at full load



Figure 59 – 85 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 10 ms / div.
Lower: 12 V I_{OUT} , 200 mA / div.
 V_{MAX} : 12.791 V.
 V_{MIN} : 11.842 V.

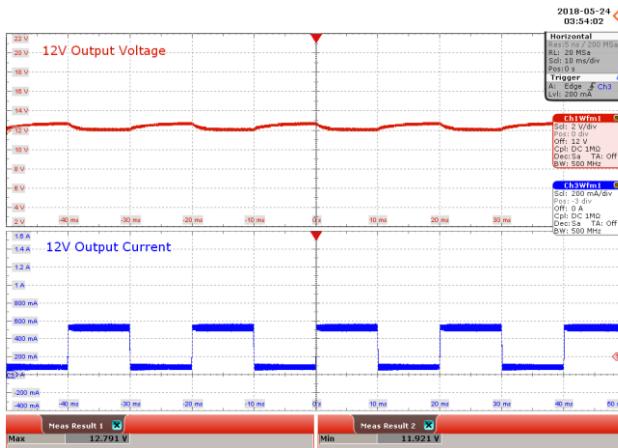


Figure 61 – 230 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 10 ms / div.
Lower: 12 V I_{OUT} , 200 mA / div.
 V_{MAX} : 12.791 V.
 V_{MIN} : 11.921 V.

Figure 60 – 115 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 10 ms / div.
Lower: 12 V I_{OUT} , 200 mA / div. V_{MAX} : 12.791 V. V_{MIN} : 11.921 V.



Figure 62 – 440 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 10 ms / div.
Lower: 12 V I_{OUT} , 200 mA / div. V_{MAX} : 12.870 V. V_{MIN} : 11.842 V.



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10.5 Fault Waveforms

10.5.1 5 V Output Short

Test conditions: Both outputs at full load before short

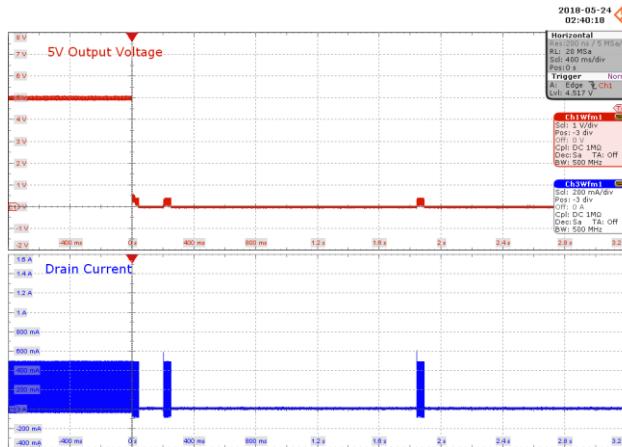


Figure 63 – 85 VAC Input.

Upper: 5 V V_{OUT} , 1 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

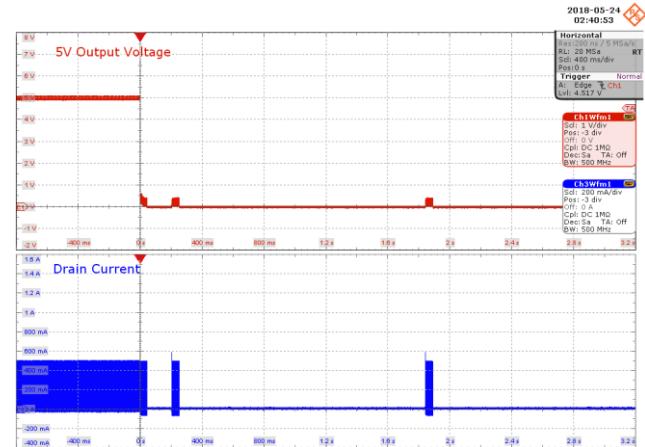


Figure 64 – 115 VAC Input.

Upper: 5 V V_{OUT} , 1 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

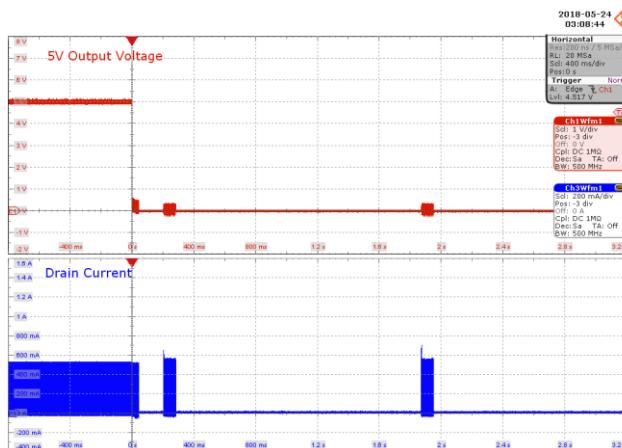


Figure 65 – 230 VAC Input.

Upper: 5 V V_{OUT} , 1 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

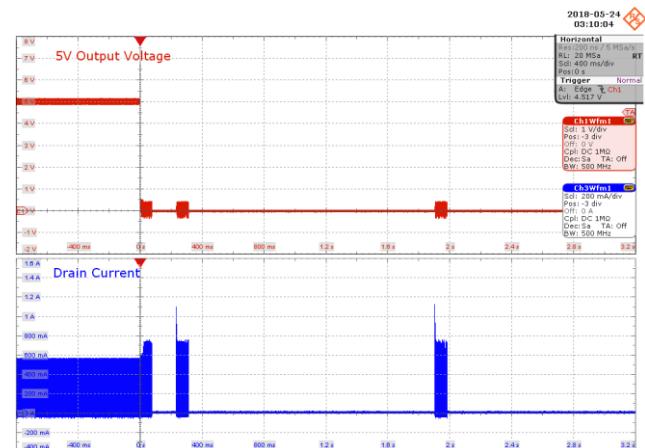


Figure 66 – 440 VAC Input.

Upper: 5 V V_{OUT} , 1 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

10.5.2 12 V Output Short

Test conditions: Both outputs at full load before short

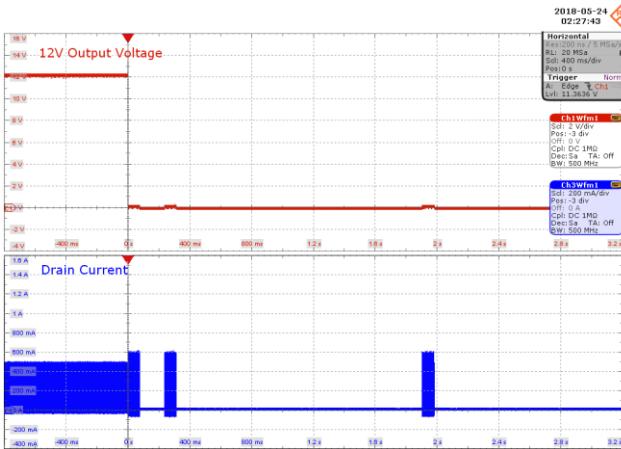


Figure 67 – 85 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

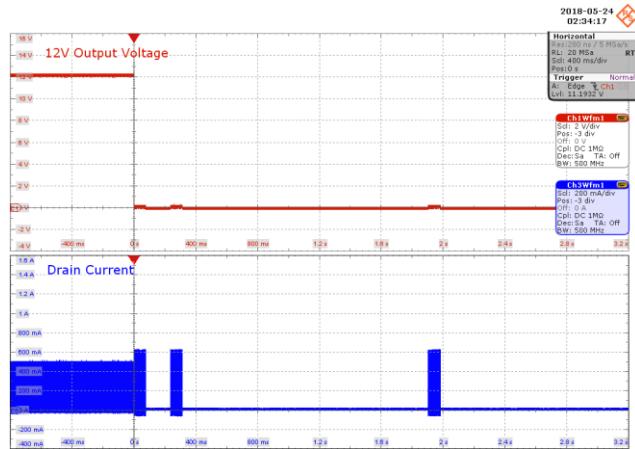


Figure 68 – 115 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

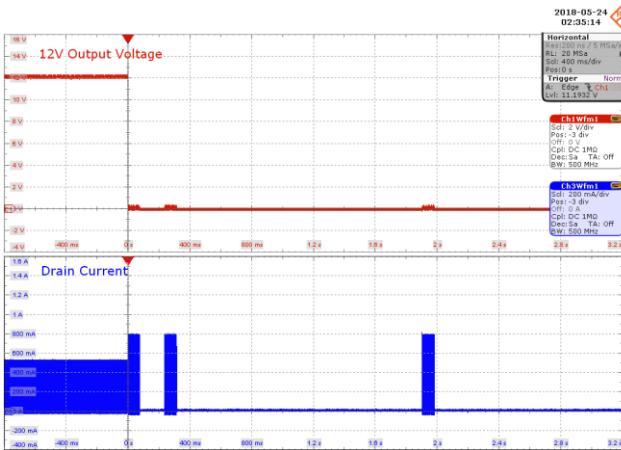


Figure 69 – 230 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.

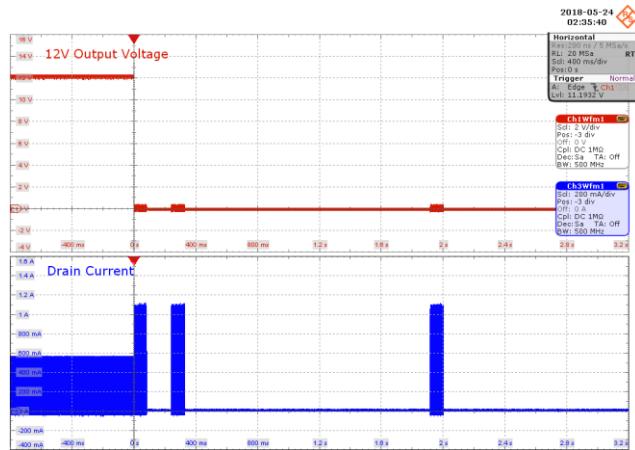


Figure 70 – 440 VAC Input.

Upper: 12 V V_{OUT} , 2 V / div., 400 ms / div.
Lower: I_{DS} , 200 mA / div.



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10.5.3 Line Overvoltage

Test conditions: VR1 Zener diode voltage rating set to 102 V, OVP at 520 VAC_{RMS}

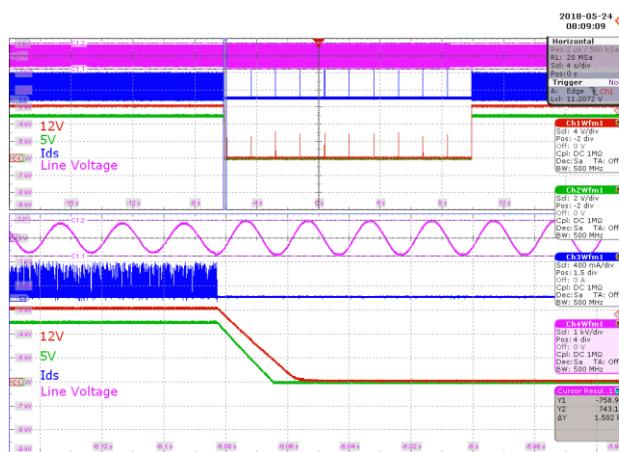


Figure 71 – Line +OV at 520 VAC_{RMS}.

Upper: 12 V V_{OUT}, 2 V / div., 400 ms / div.
Lower: I_{DS}, 200 mA / div.

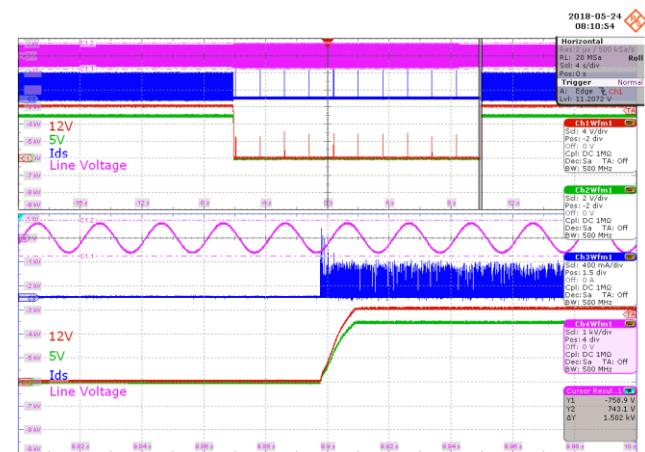


Figure 72 – Line -OV.

Upper: 12 V V_{OUT}, 2 V / div., 400 ms / div.
Lower: I_{DS}, 200 mA / div.

11 Thermal Performance

11.1 Test Set-Up

Thermal evaluation was performed under two conditions: (1) room temperature with the circuit board enclosed inside an acrylic box and (2), 50 °C ambient inside a thermal chamber. In both conditions, the circuit is soaked for two hours under full load conditions.

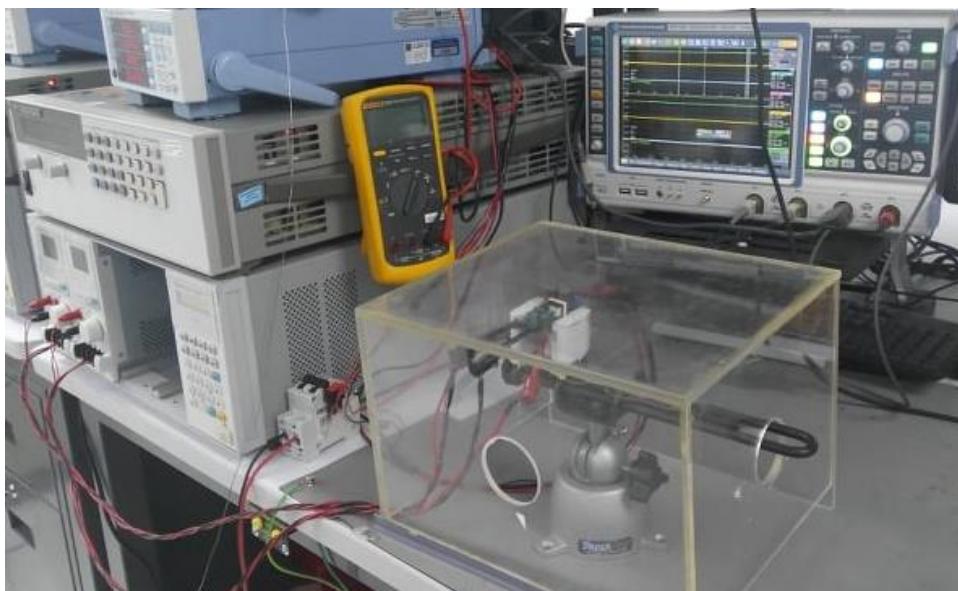


Figure 73 – Thermal Performance Set-up Using an Acrylic Box.



Figure 74 – Thermal Performance Set-up Using Thermal Chamber.



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11.2 Room Temperature

11.2.1 85 VAC @ Room Temperature

Ambient (°C)	LinkSwitch-XT2 900 V (U1)	Transformer (T1)	12 V Output Diode (T2)	Bridge Rectifier (BR1)
27	53.3	60.0	71.0	47.3

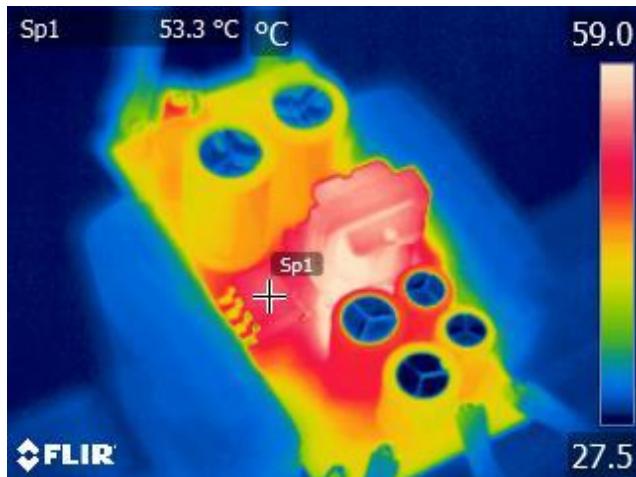


Figure 75 – Ambient = 27.5 °C.
LNK-XT2-900, U1 = 53.3 °C.

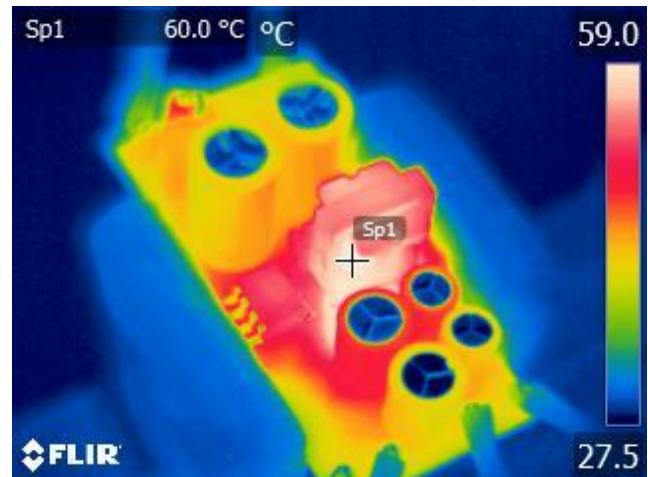


Figure 76 – Ambient = 27.5 °C.
Transformer, T1 = 60.0 °C.

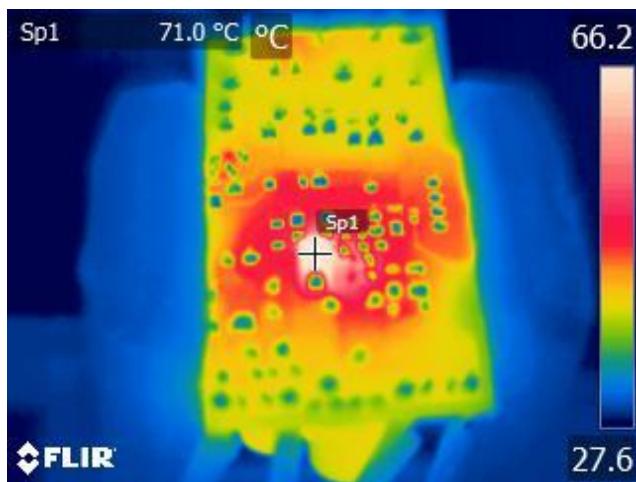


Figure 77 – Ambient = 27.6 °C.
12 V Diode, D4 = 71.0 °C.

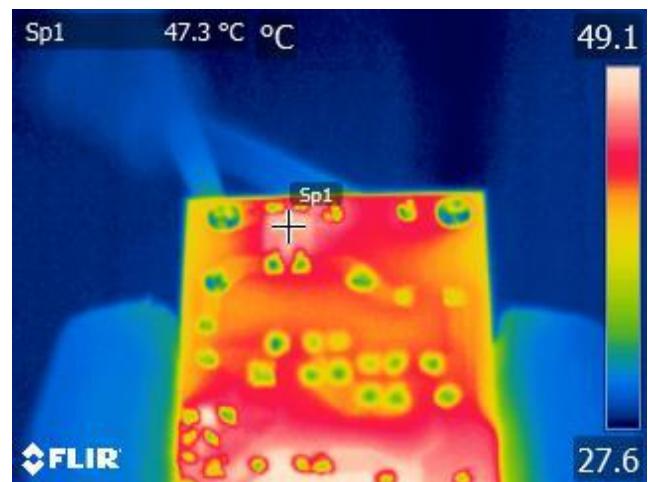


Figure 78 – Ambient = 27.6 °C.
Bridge Rectifier, BR1 = 47.3 °C.

11.2.2 440 VAC @ Room Temperature

Ambient (°C)	LinkSwitch-XT2 900 V (U1)	Transformer (T1)	12 V Output Diode (T2)	Bridge Rectifier (BR1)
27	54.6	63.1	78.4	37.0

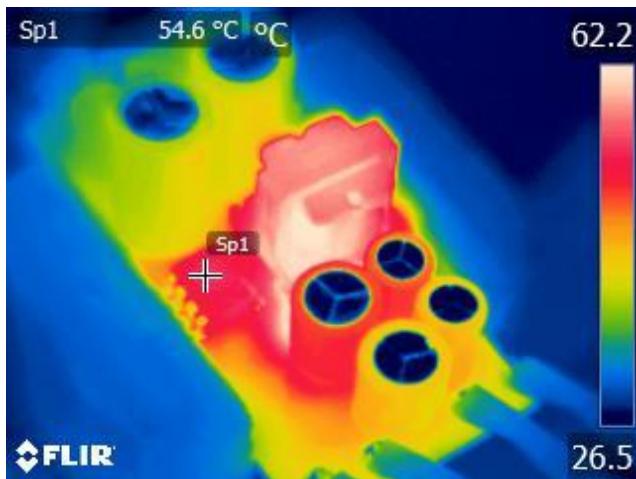


Figure 79 – Ambient = 26.5 °C.
LNK-XT2-900, U1 = 54.6 °C.

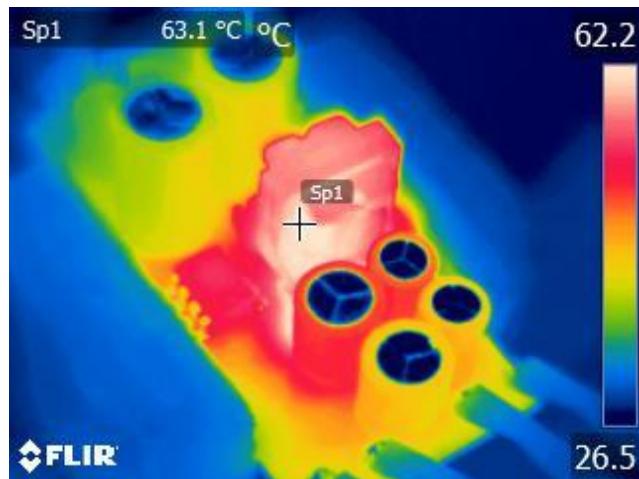


Figure 80 – Ambient = 26.5 °C.
Transformer, T1 = 63.1 °C.

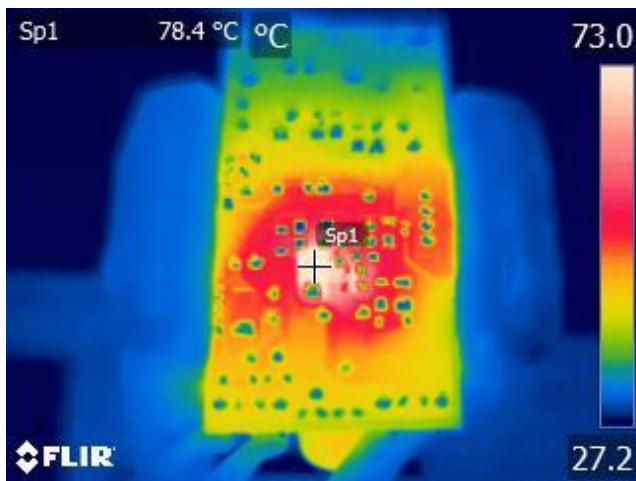


Figure 81 – Ambient = 27.2 °C.
12 V Diode, D4 = 78.4 °C.

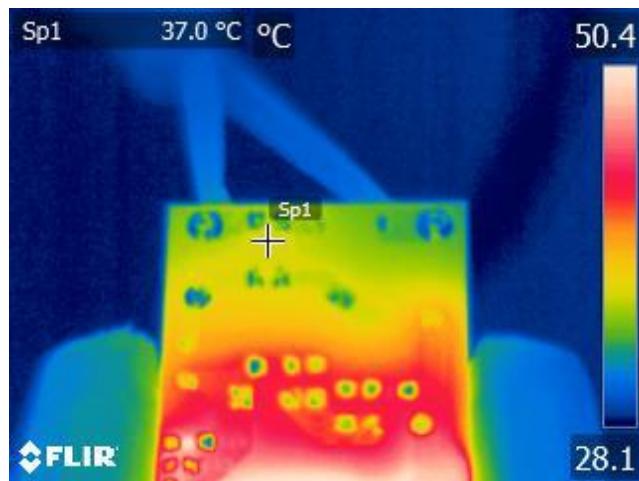


Figure 82 – Ambient = 28.1 °C.
Bridge Rectifier, BR1 = 37.0 °C.

11.3 50 °C Ambient

11.3.1 85 VAC @ 50 °C

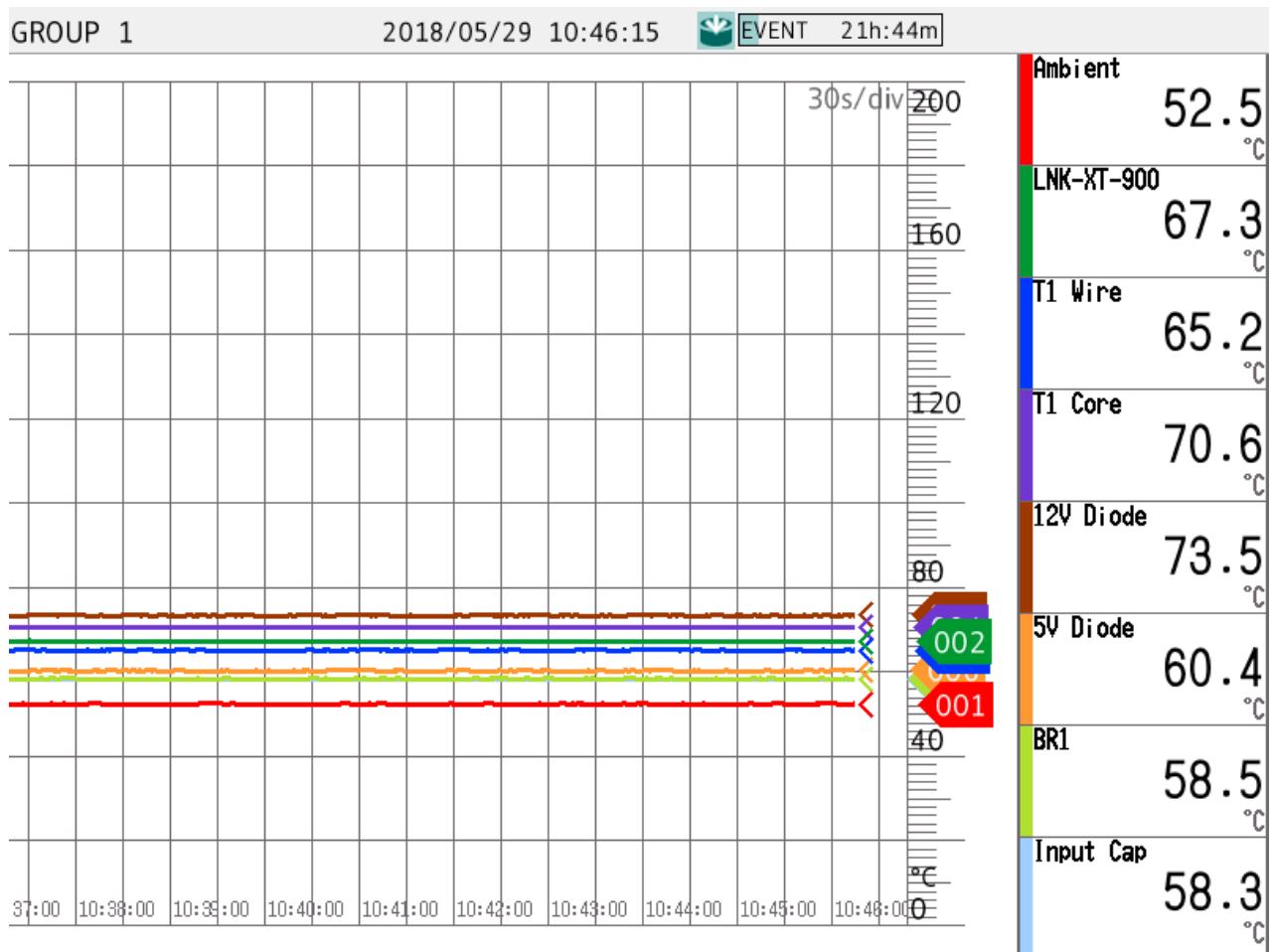
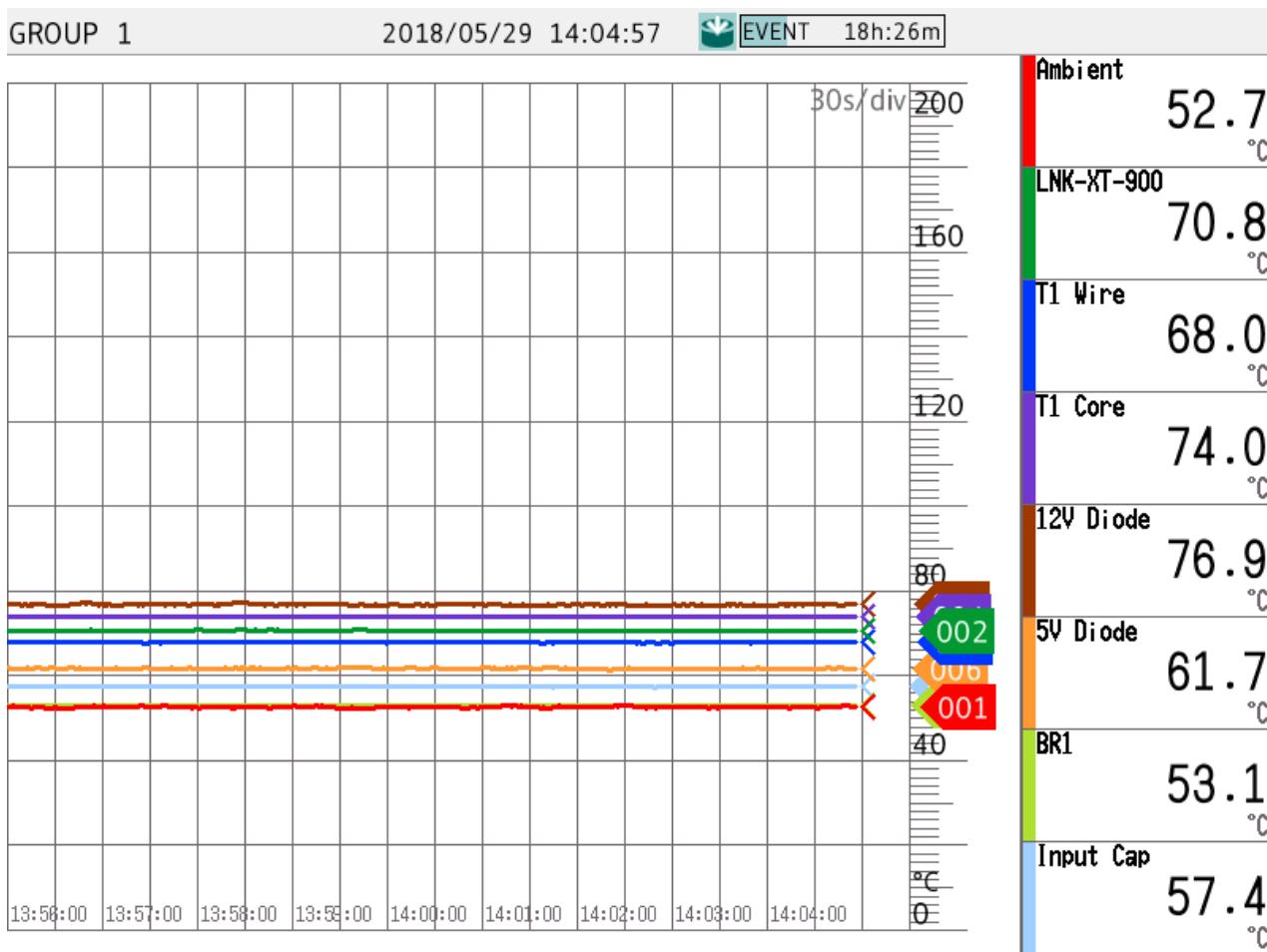


Figure 83 – Component Temperatures at 50 °C Ambient.

11.3.2 440 VAC @ 50 °C

**Figure 84 — Component Temperatures at 50 °C Ambient.**

12 Conducted EMI

12.1 EMI Equipment and Load

1. Rohde and Schwarz ENV216 two line V-network.
2. Rohde and Schwarz ESRP EMI test receiver.
3. Hioki 3322 power hitester.
4. Chroma measurement test fixture, model A662003.
5. Resistor load with input voltage set at 115 VAC.

12.2 Test Set-up

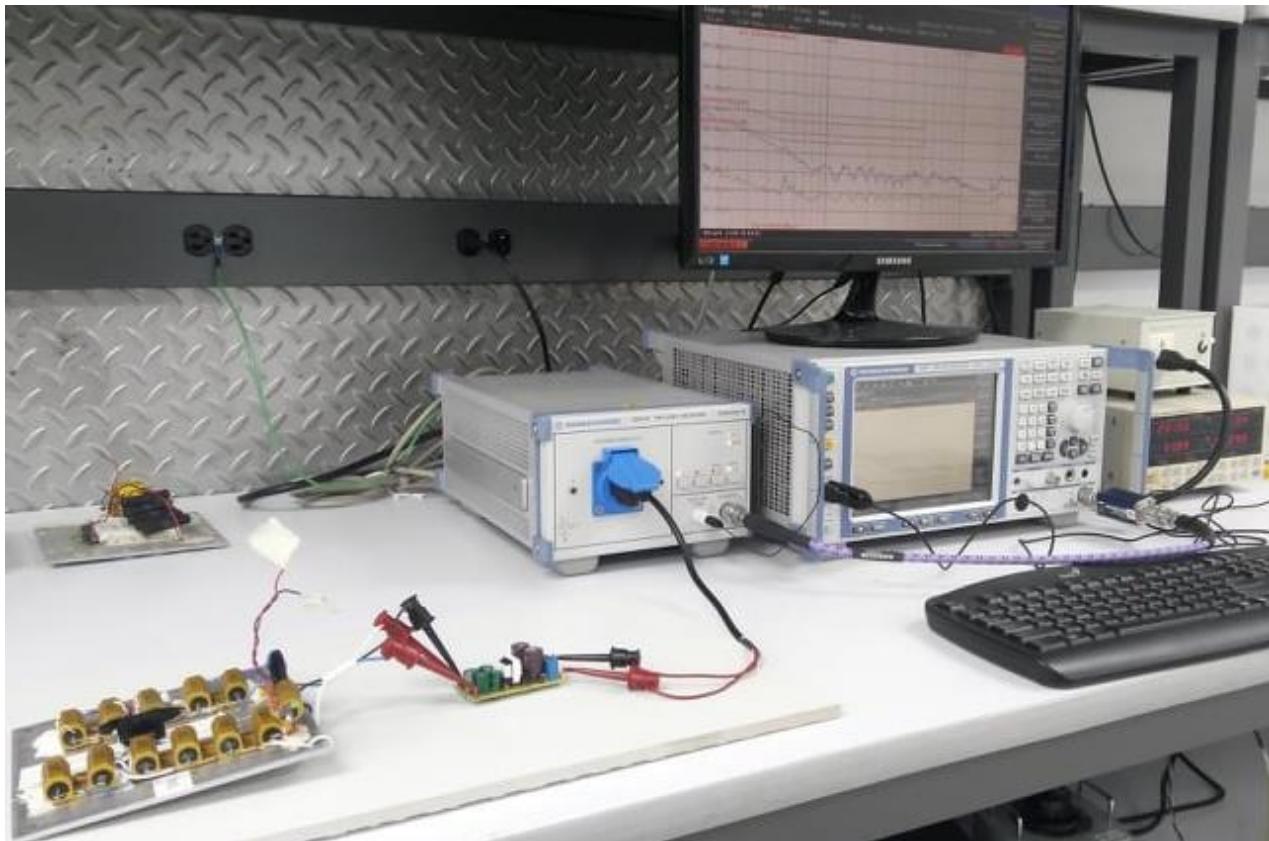
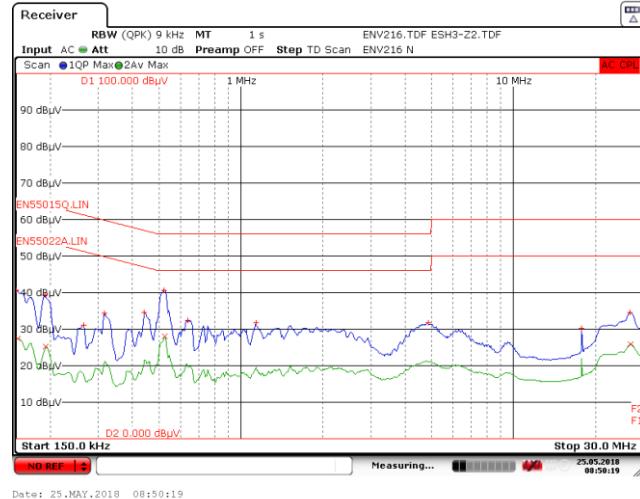
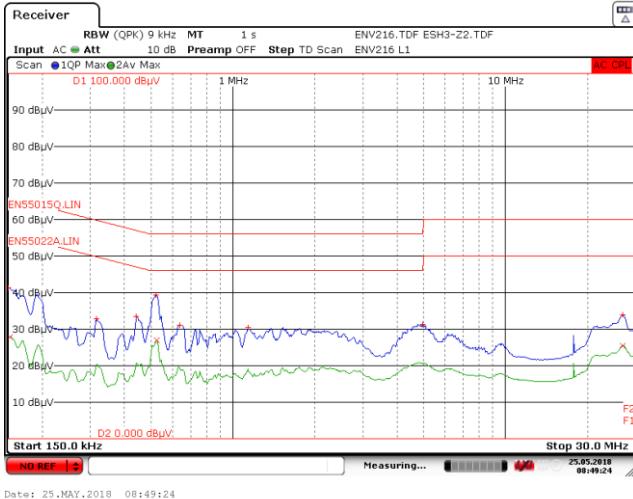


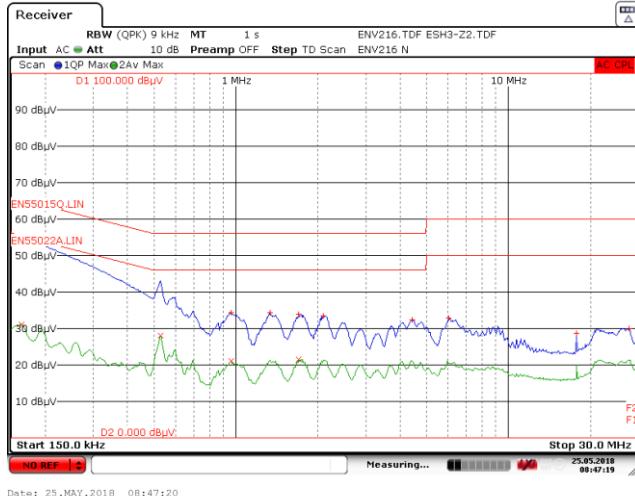
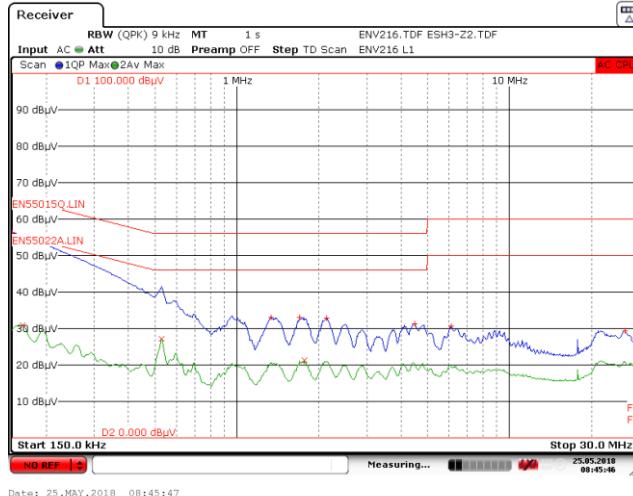
Figure 85 — Conducted EMI Test Set-up.

12.3 EMI Test Results

12.3.1 115 VAC, Floating Output



12.3.2 230 VAC, Floating Output



13 Line Surge

The unit was subject to ± 2000 V, 100 kHz ring wave, and ± 1000 V differential surge test using 10 strikes at each condition. A test failure is defined as a non-recoverable interruption of output requiring repair or recycling of input voltage.

13.1 Differential Surge Test

Surge Voltage (kV)	Phase Angle (°)	IEC Coupling	Generator Impedance (Ω)	Number Strikes	Result
+1	0	L1 / L2	2	10	PASS
-1	0	L1 / L2	2	10	PASS
+1	90	L1 / L2	2	10	PASS
-1	90	L1 / L2	2	10	PASS
+1	180	L1 / L2	2	10	PASS
-1	180	L1 / L2	2	10	PASS
+1	270	L1 / L2	2	10	PASS
-1	270	L1 / L2	2	10	PASS

Note: In all PASS results, no damage and no auto-restart was observed.

13.2 Ring Wave Test

Ring Wave Voltage (kV)	Phase Angle (°)	IEC Coupling	Generator Impedance (Ω)	Number Strikes	Result
+2	0	L1 / L2	12	10	PASS
-2	0	L1 / L2	12	10	PASS
+2	90	L1 / L2	12	10	PASS
-2	90	L1 / L2	12	10	PASS
+2	180	L1 / L2	12	10	PASS
-2	180	L1 / L2	12	10	PASS
+2	270	L1 / L2	12	10	PASS
-2	270	L1 / L2	12	10	PASS

Note: In all PASS results, no damage and no auto-restart was observed.

14 Revision History

Date	Author	Revision	Description & Changes	Reviewed
26-Sep-18	IB & JPB	1.0	Initial Release.	Mktg & Apps
26-Oct-18	IB	1.1	Updated Section 8 Transformer Design Spreadsheet.	Mktg & Apps
30-Jun-20	KM	1.2	Updated Transformer Assembly Section. Converted to RDR	Mktg & Apps

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WORLD HEADQUARTERS

5245 Hellyer Avenue
San Jose, CA 95138, USA.
Main: +1-408-414-9200
Customer Service:
Phone: +1-408-414-9665
Fax: +1-408-414-9765
e-mail: usasales@power.com

GERMANY

(IGBT Driver Sales)
HellwegForum 1
59469 Ense, Germany
Tel: +49-2938-64-39990
Email: igbt-driver.sales@power.com

KOREA

RM 602, 6FL
Korea City Air Terminal B/D,
159-6
Samsung-Dong, Kangnam-Gu,
Seoul, 135-728 Korea
Phone: +82-2-2016-6610
Fax: +82-2-2016-6630
e-mail: koreasales@power.com

CHINA (SHANGHAI)

Rm 2410, Charity Plaza, No.
88,
North Caoxi Road,
Shanghai, PRC 200030
Phone: +86-21-6354-6323
Fax: +86-21-6354-6325
e-mail:
chinasales@power.com

INDIA

#1, 14th Main Road
Vasanthanagar
Bangalore-560052
India
Phone: +91-80-4113-8020
Fax: +91-80-4113-8023
e-mail:
indiasales@power.com

SINGAPORE

51 Newton Road,
#19-01/05 Goldhill Plaza
Singapore, 308900
Phone: +65-6358-2160
Fax: +65-6358-2015
e-mail:
singaporesales@power.com

CHINA (SHENZHEN)

17/F, Hivac Building, No. 2, Keji
Nan 8th Road, Nanshan District,
Shenzhen, China, 518057
Phone: +86-755-8672-8689
Fax: +86-755-8672-8690
e-mail: chinasales@power.com

ITALY

Via Milanese 20, 3rd. Fl.
20099 Sesto San Giovanni (MI)
Italy
Phone: +39-024-550-8701
Fax: +39-028-928-6009
e-mail: eurosales@power.com

TAIWAN

5F, No. 318, Nei Hu Rd.,
Sec. 1
Nei Hu District
Taipei 11493, Taiwan R.O.C.
Phone: +886-2-2659-4570
Fax: +886-2-2659-4550
e-mail: taiwansales@power.com

GERMANY

(AC-DC/LED Sales)
Lindwurmstrasse 114
80337, Munich
Germany
Phone: +49-895-527-39110
Fax: +49-895-527-39200
e-mail: eurosales@power.com

JAPAN

Kosei Dai-3 Building
2-12-11, Shin-Yokohama,
Kohoku-ku, Yokohama-shi,
Kanagawa 222-0033
Japan
Phone: +81-45-471-1021
Fax: +81-45-471-3717
e-mail: japansales@power.com

UK

Cambridge Semiconductor,
a Power Integrations company
Westbrook Centre, Block 5, 2nd
Floor
Milton Road
Cambridge CB4 1YG
Phone: +44 (0) 1223-446483
e-mail: eurosales@power.com

